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UWB Double-Directional Channel Sounding

- Why and how? -

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- Antennas and propagation in UWB
- Propagation issues relating with MIMO
- UWB double directional channel sounding
- Evaluation and modeling issues of sounding technology

Ultra Wideband Radio

- FCC definition in US
 - 20% or 500MHz
 - 3.1GHz ~ 10.6GHz
 - -41.3dBm

Spread spectrum

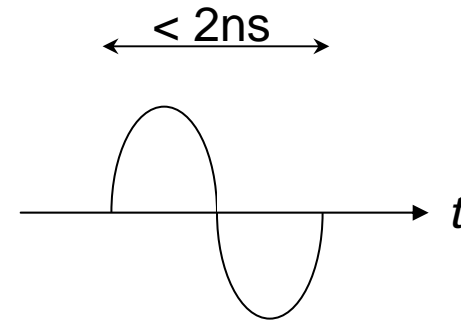
Avoid dense application

Coexistence

Trend of UWB – IEEE 802.15.3a

Impulse radio

- Simple hardware
- Low power consumption

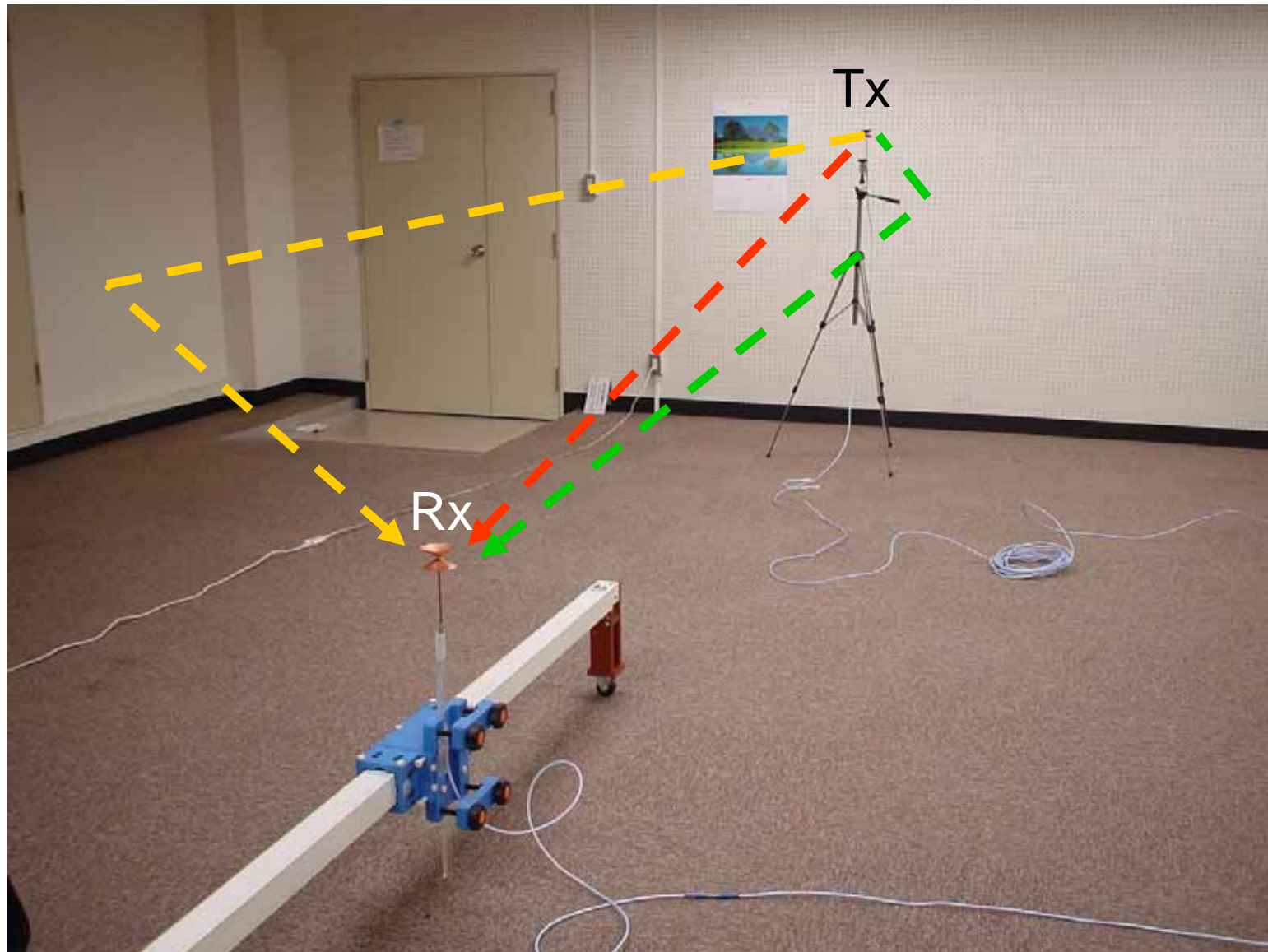


IEEE 802.15 TG3a : High Speed Personal Area Network

DS-CDMA

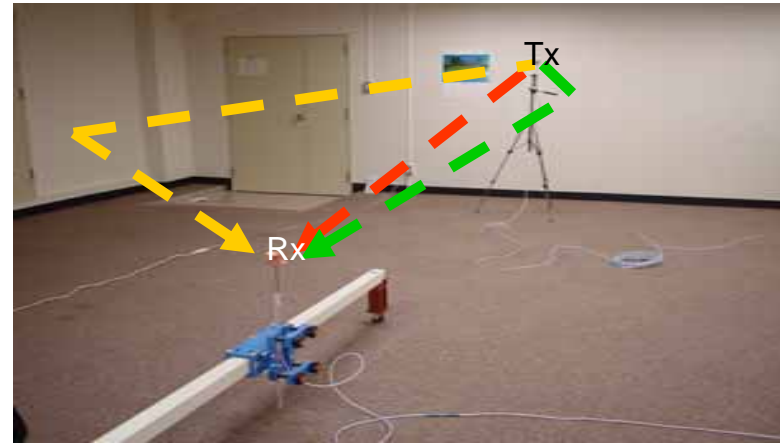
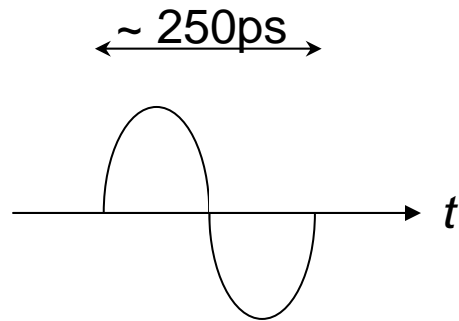
MB-OFDM

Indoor Multipath Environment

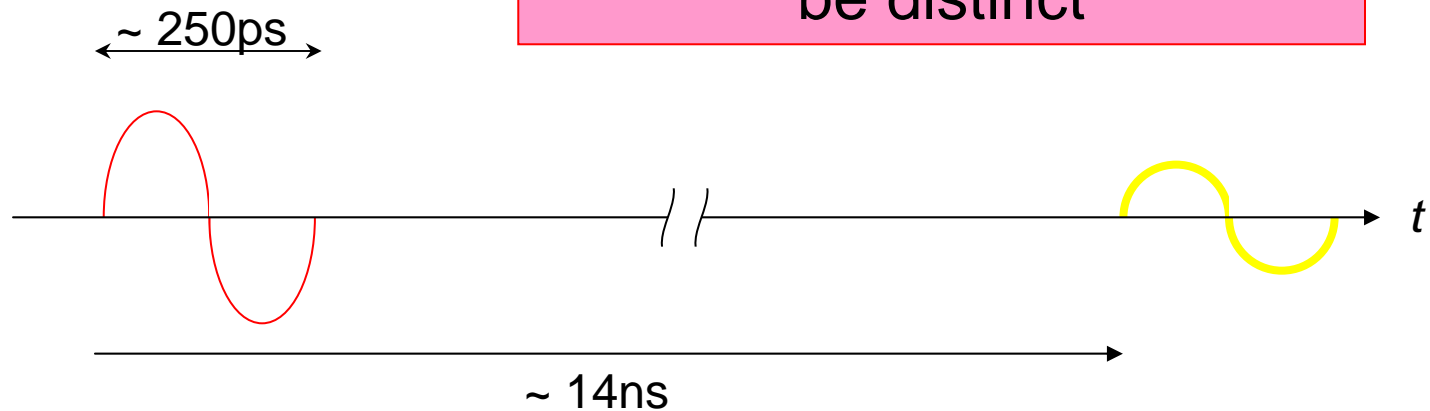


Transmission in Multipath Environment

Tx pulse (4GHz BW)

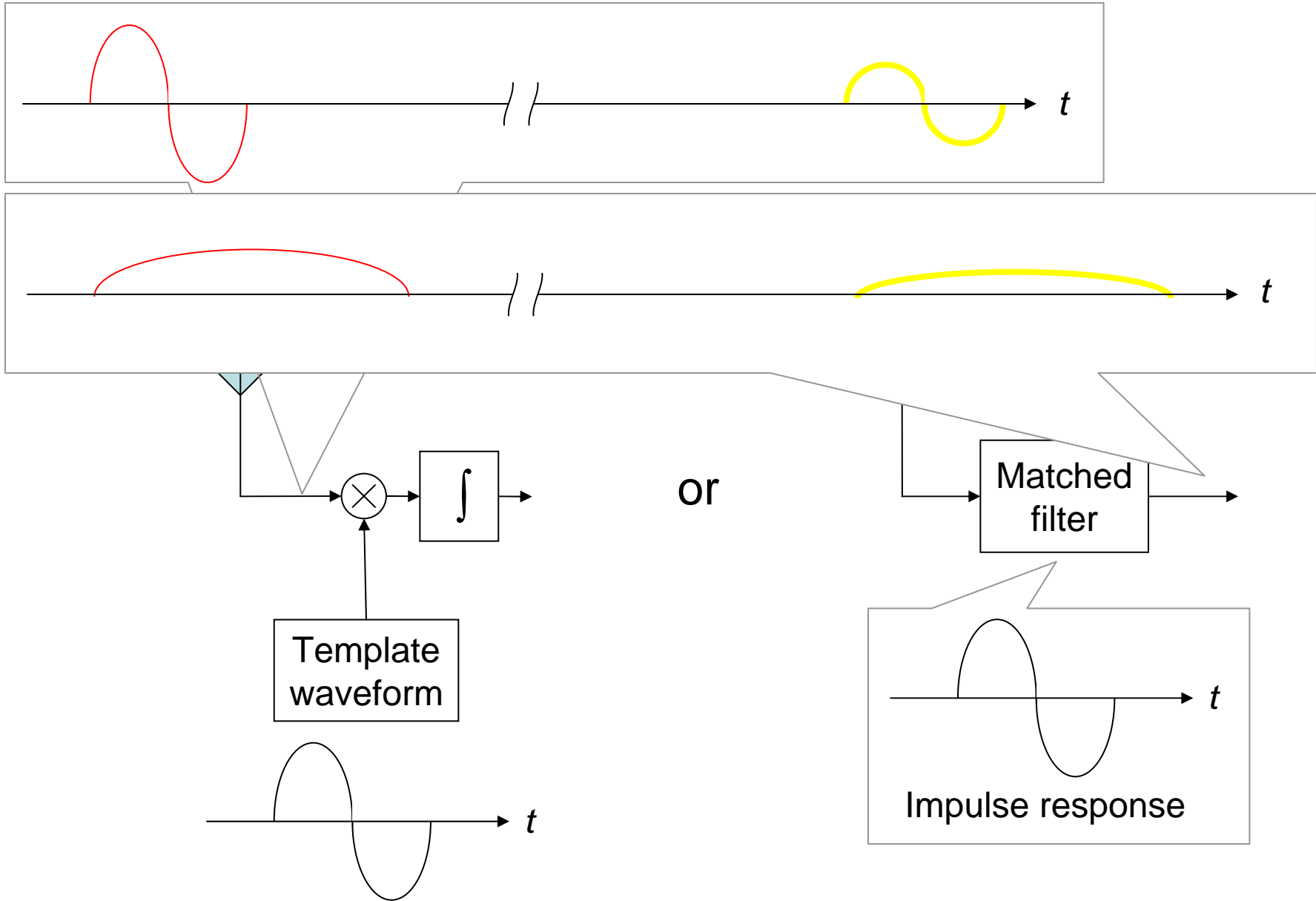


Rx pulse



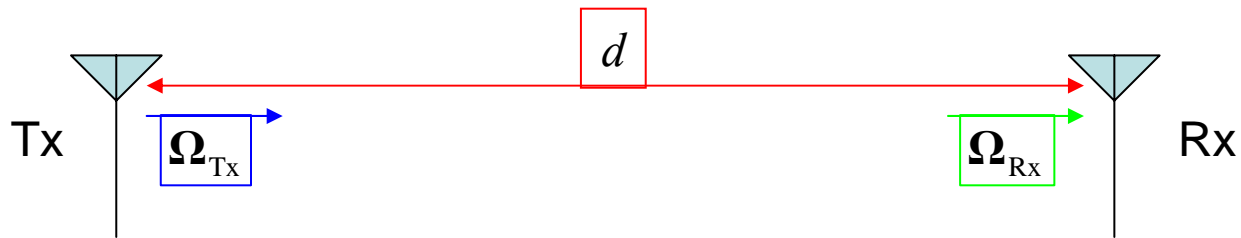
Multipath components can be distinct

UWB Receiver



Free Space Transfer Function

- Friis' transmission formula



$$H_{\text{Friis}}(f) = H_{\text{FreeSpace}}(f, d) \mathbf{H}_{\text{Tx}}(f, \mathbf{\Omega}_{\text{Tx}}) \cdot \mathbf{H}_{\text{Rx}}(f, \mathbf{\Omega}_{\text{Rx}})$$

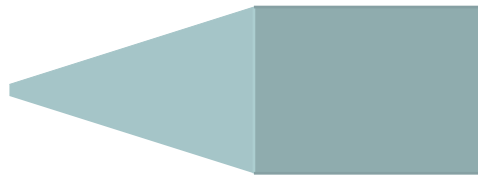
$\propto \frac{1}{f}$

Normalized by
isotropic antenna

Ideal Antenna Cases

- Constant aperture size

Example : Pyramidal horn



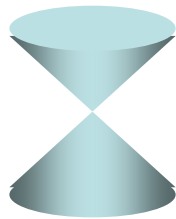
$$H_{\text{Ant}} \propto f$$



$$H_{\text{Friis}} \propto f$$

- Constant gain

Example : Biconical



$$H_{\text{Ant}} \doteq \text{const.}$$

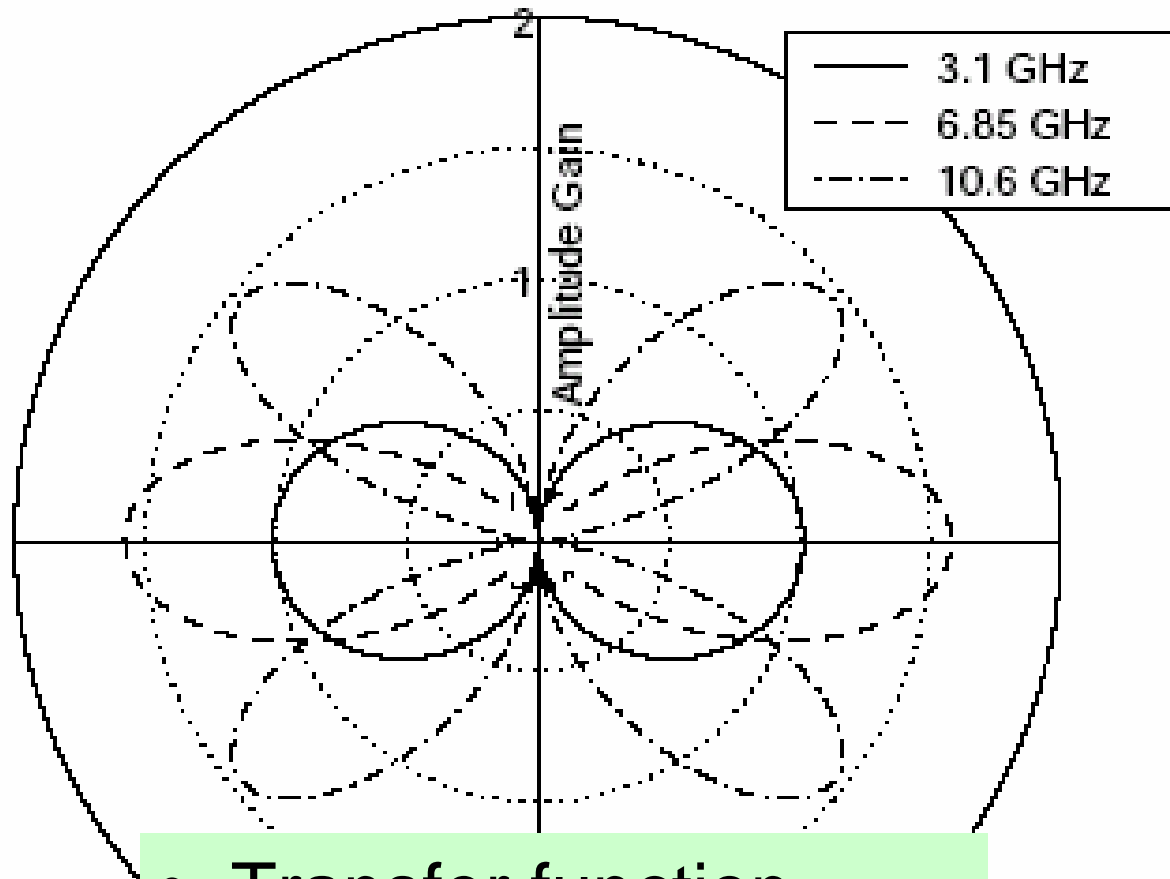


$$H_{\text{Friis}} \propto \frac{1}{f}$$

Both are
too idealized

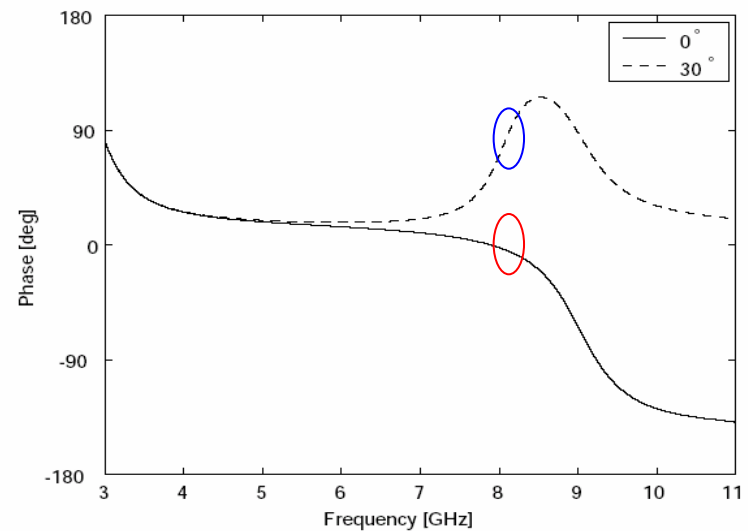
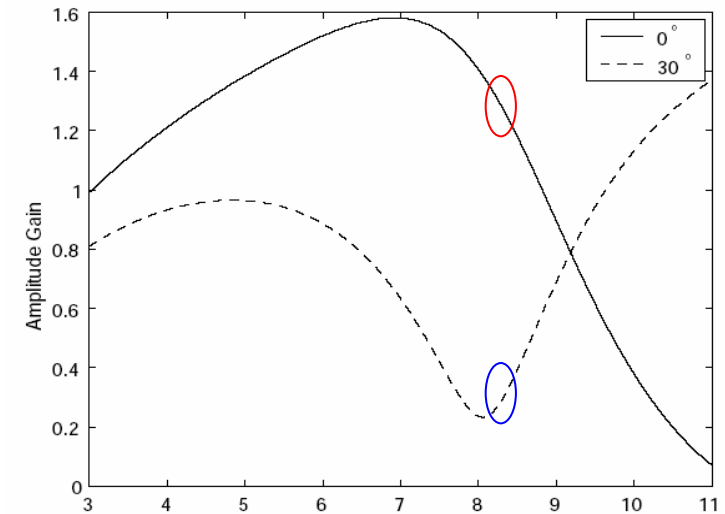
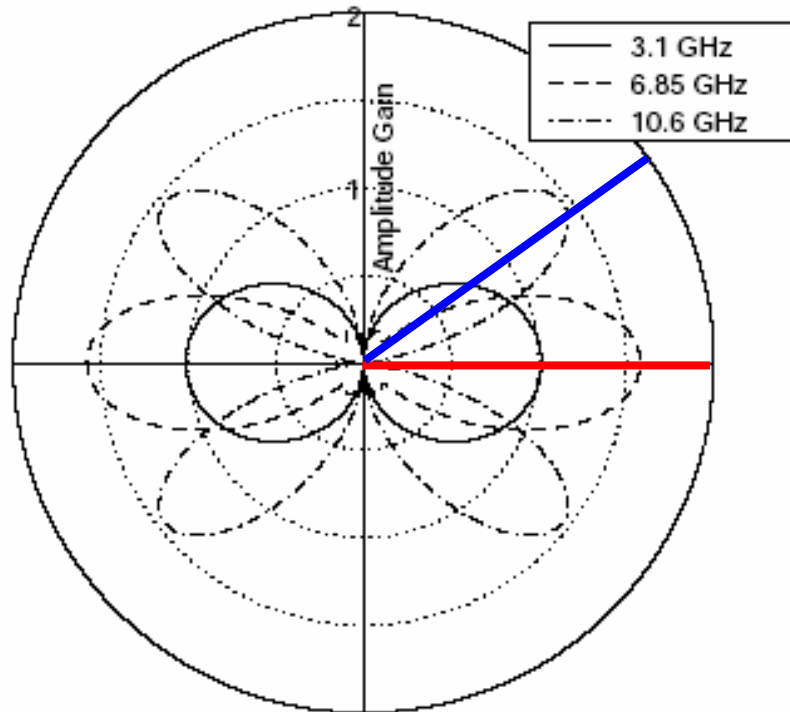
Frequency Characteristics of Antenna

4.8cm Dipole (resonant at 3.1GHz)



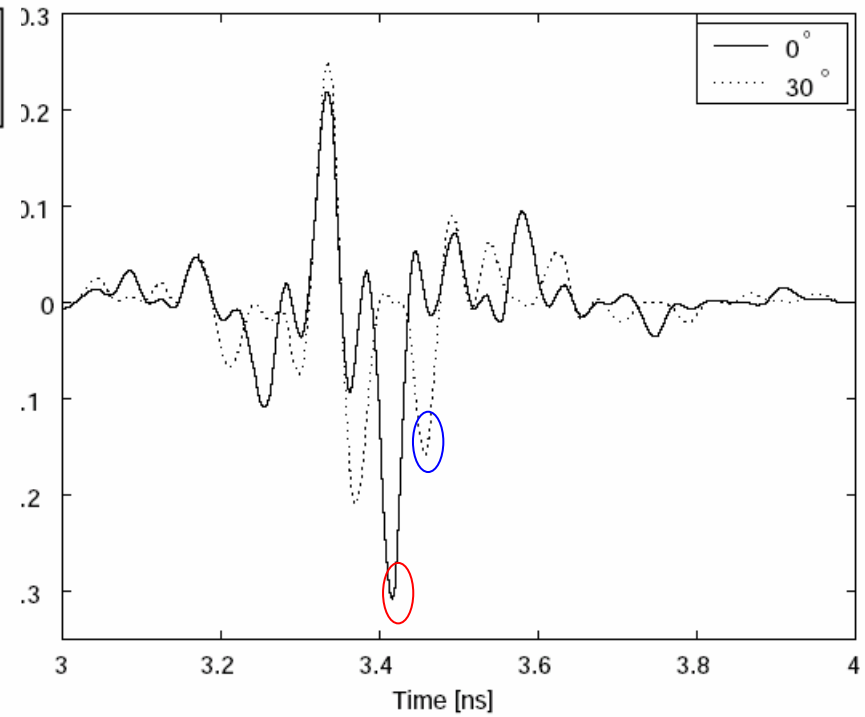
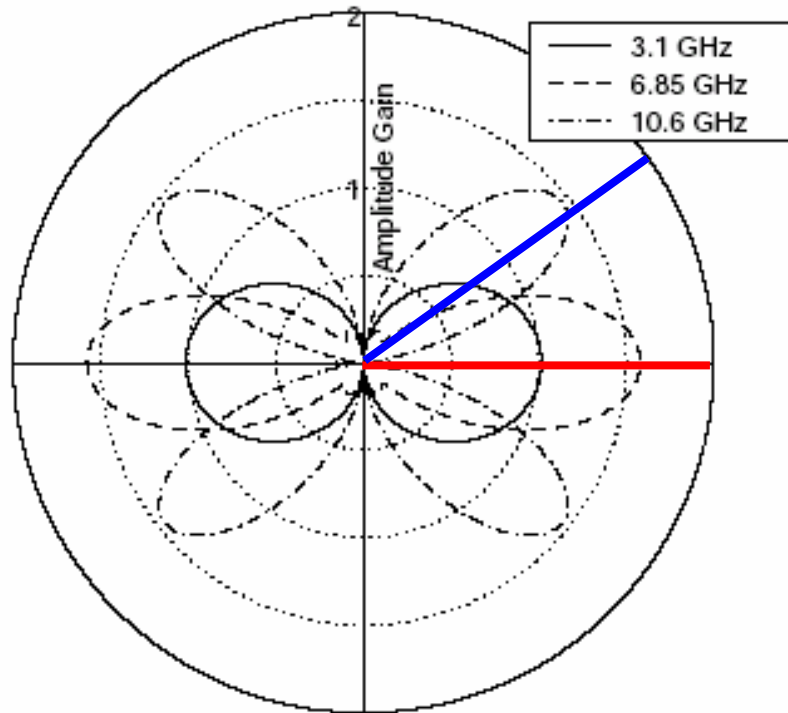
- Transfer function
 - Frequency dependent
 - Angular dependent

Directional Transfer Function of Antenna



Drastically changed by direction

Directional Impulse Response of Antenna



↔
0.2ns

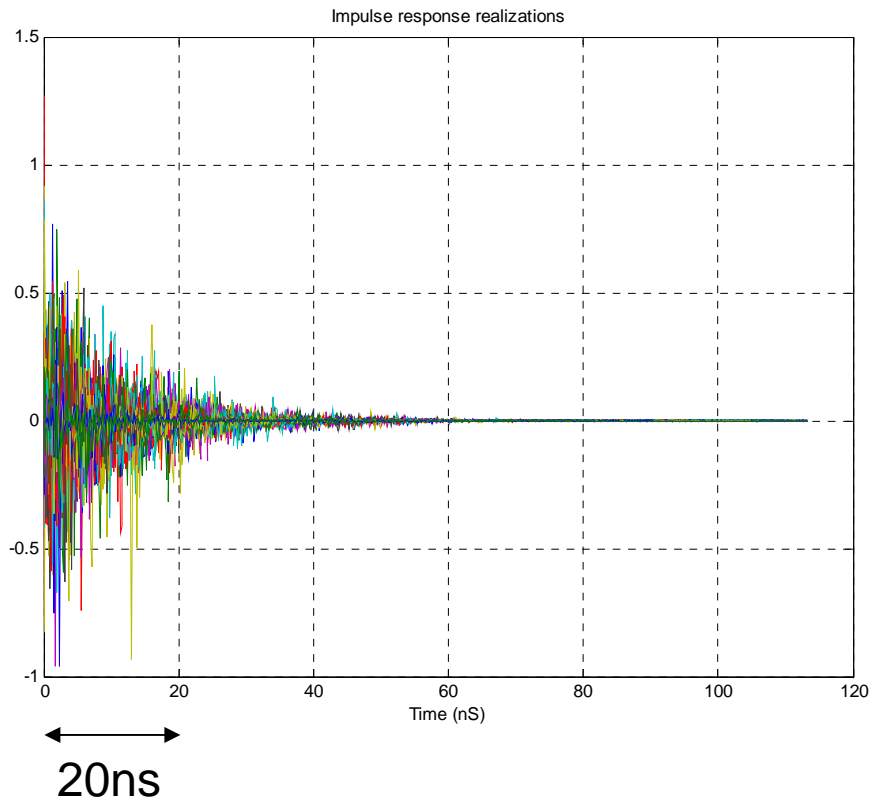
Conventional System vs UWB

Antenna and propagation issues

| | Conventional systems | UWB-IR |
|-----------|--------------------------|-------------|
| Antenna | Gain (frequency flat) | Distortion |
| Multipath | Distortion | Distinction |

Conventional Channel Model

IEEE 802.15.3a Model

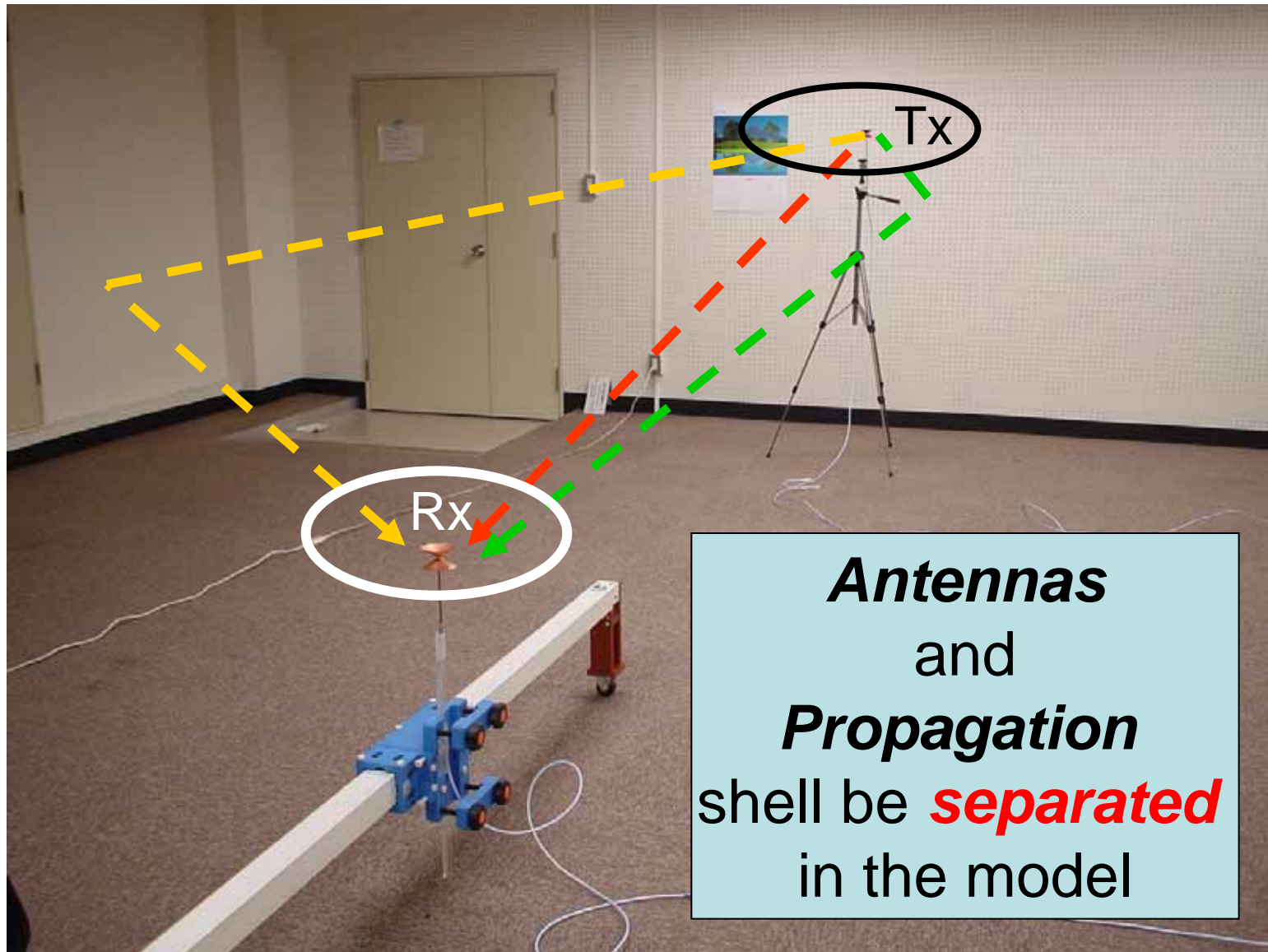


Channel includes
antennas and
propagation



Valid only for test
antennas (omni) !

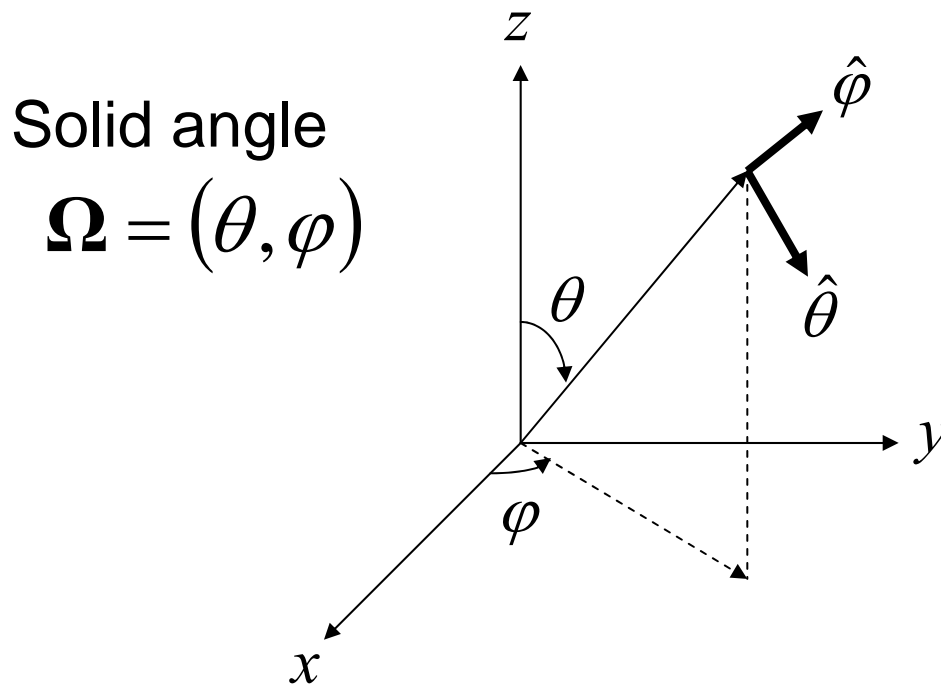
Channel Modeling Approach of UWB



Antenna Model Parameters

Directive Polarimetric Frequency Transfer Function

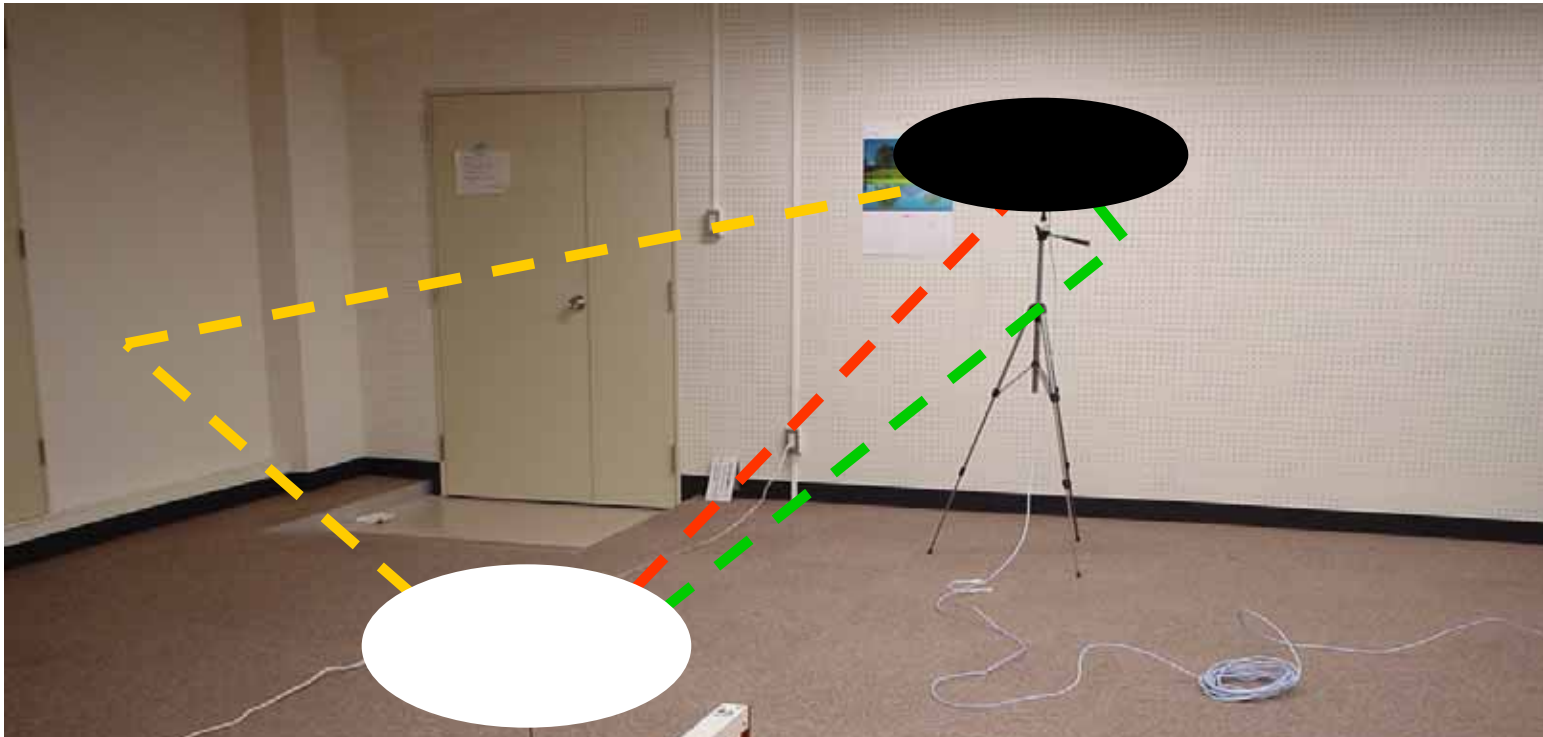
$$\mathbf{H}_{\text{Ant}}(f, \theta, \varphi) = \hat{\boldsymbol{\theta}}(\theta, \varphi) H_{\theta, \text{Ant}}(f, \theta, \varphi) + \hat{\boldsymbol{\phi}}(\theta, \varphi) H_{\phi, \text{Ant}}(f, \theta, \varphi)$$



How to Get Antenna Model Parameters

- Electromagnetic (EM) wave simulator
 - MoM (NEC, FEKO, ...)
 - FEM (HFSS, ...)
 - FDTD (XFDTD, ...)
 - ...
- Spherical polarimetric measurement
 - Three antenna method for testing antenna calibration

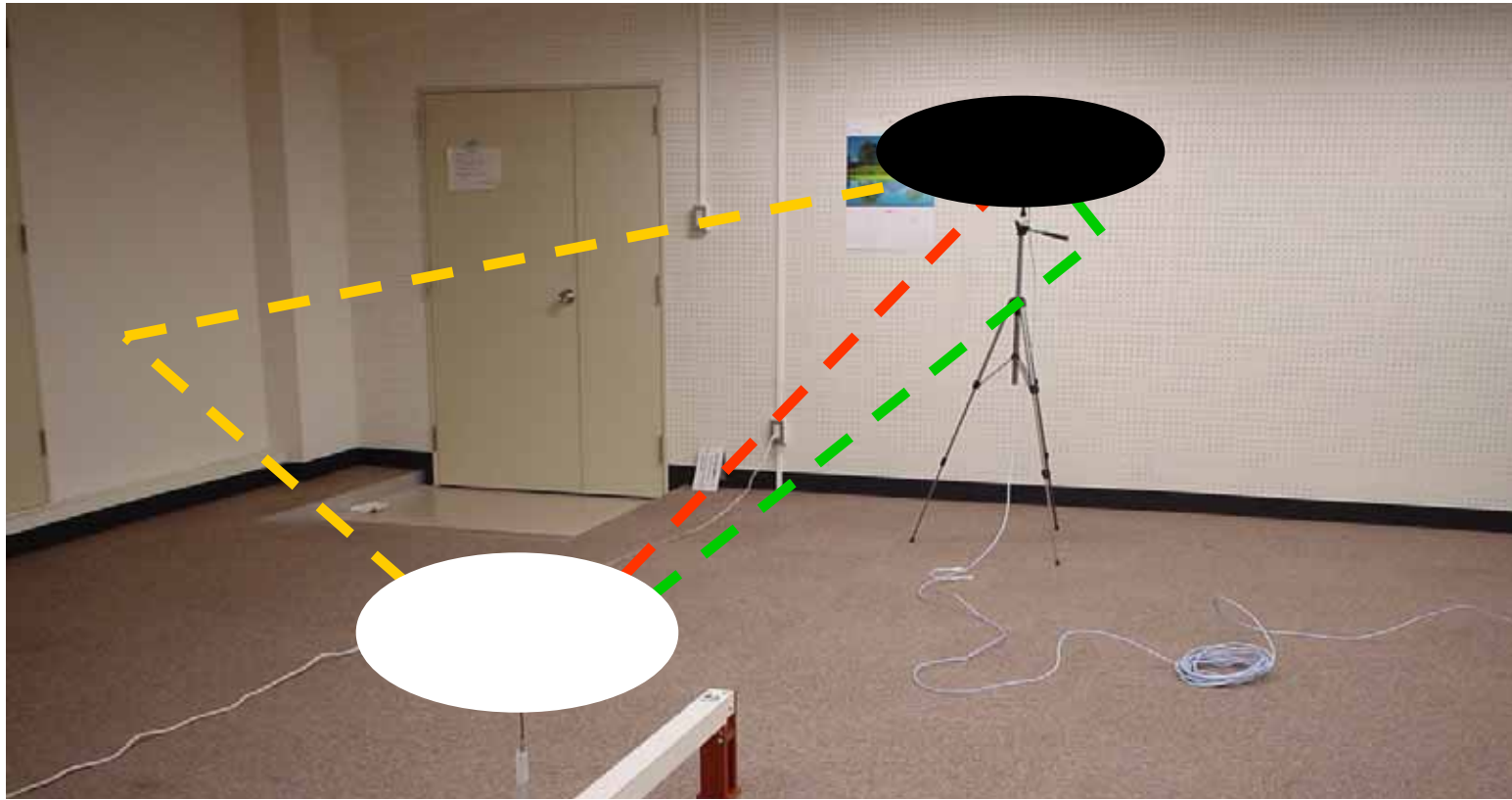
Propagation Modeling



Double-directional model

- Direction of departure (DoD)
- Direction of arrival (DoA)
- Delay time (DT)
- Magnitude (polarimetric, **frequency dependent**)

Double Directional Ray Model

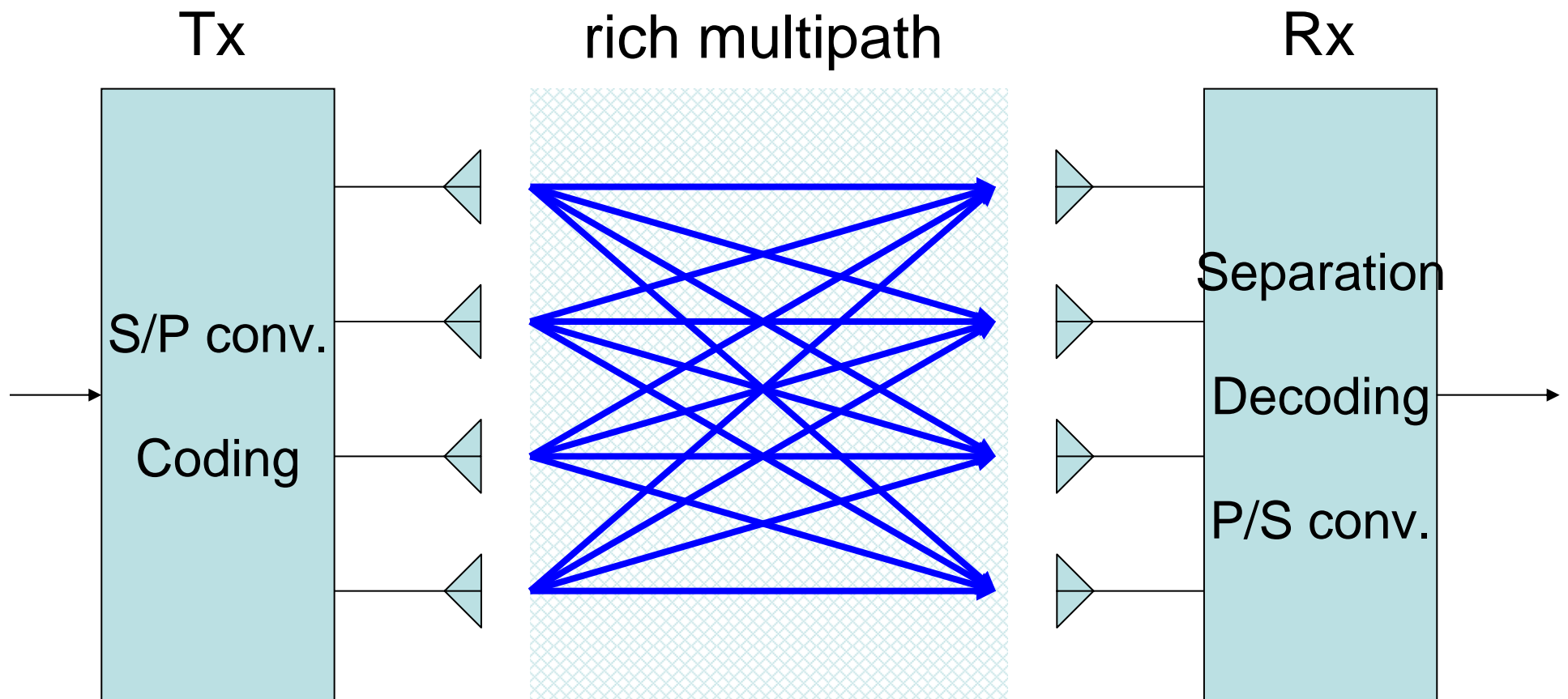


$$H_{\text{Multipath}}(f, \boldsymbol{\Omega}_{\text{Tx}}, \boldsymbol{\Omega}_{\text{Rx}}) =$$

$$\sum_{l=1}^L a_l(f) \delta(\boldsymbol{\Omega}_{\text{Tx}} - \boldsymbol{\Omega}_{\text{Tx},l}) \delta(\boldsymbol{\Omega}_{\text{Rx}} - \boldsymbol{\Omega}_{\text{Rx},l}) \exp(-j2\pi f \tau_l)$$

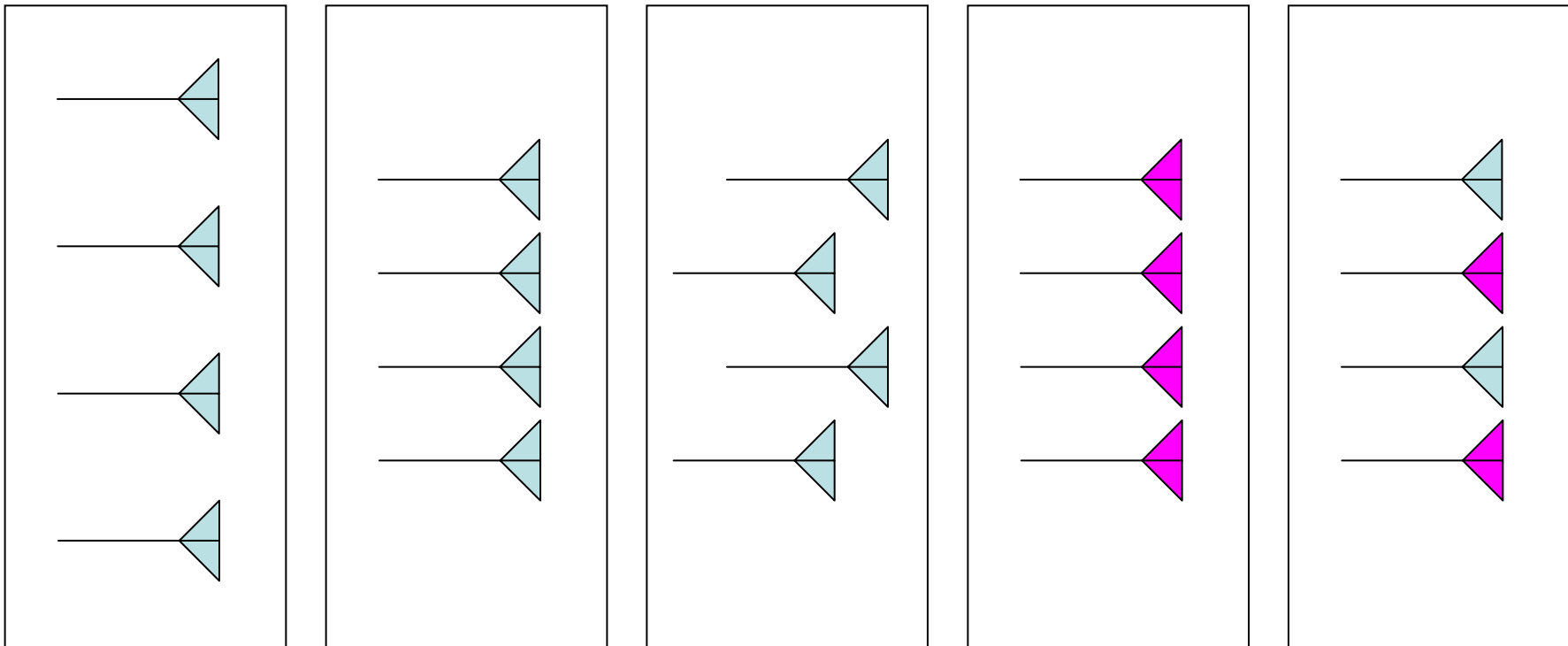
Double Directional Channel Model

... has been studied for MIMO systems

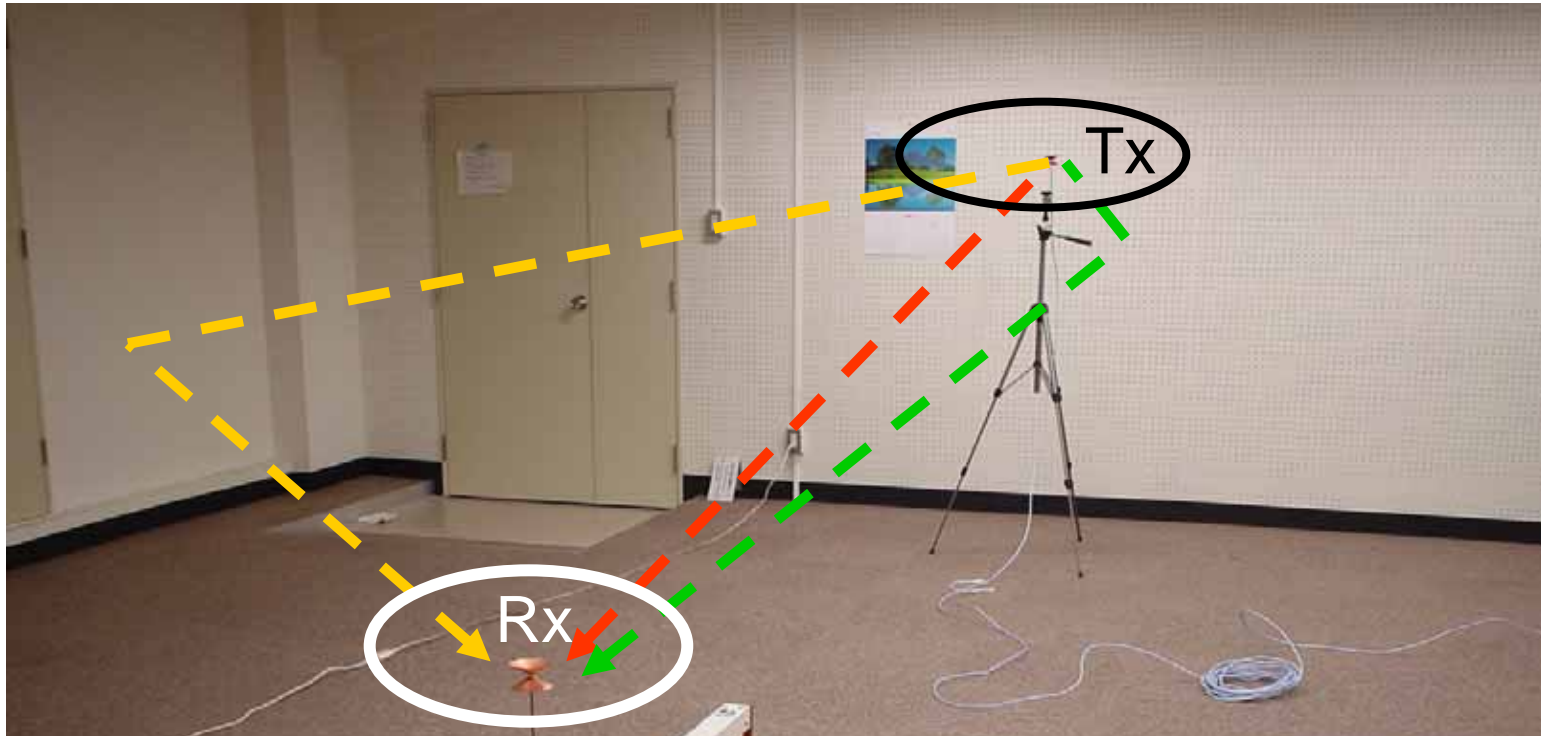


MIMO Antennas

Design of array antenna is a key issue of MIMO channel capacity.



MIMO Channel Matrix



$$\overline{\overline{H}}(f) = \text{Rx antenna array vector}$$

$$\iint_{\Omega_{Tx}} \iint_{\Omega_{Rx}} \overline{H}_{Rx}(f, \boldsymbol{\Omega}_{Rx}) H_{\text{Multipath}}(f, \boldsymbol{\Omega}_{Tx}, \boldsymbol{\Omega}_{Rx}) \overline{H}_{Tx}^H(f, \boldsymbol{\Omega}_{Tx}) d\boldsymbol{\Omega}_{Rx} d\boldsymbol{\Omega}_{Tx}$$

Tx antenna array vector

MIMO vs UWB

Antenna and propagation issues

| | MIMO | UWB-IR |
|-----------|---------------------|----------------------|
| Antenna | Array configuration | Frequency distortion |
| Multipath | Double directional | |
| Magnitude | Frequency flat | Frequency dispersive |

Propagation modeling approaches are the same.



UWB Channel Sounding

Time domain vs Frequency domain

| | Time domain (Pulse) | Frequency domain (VNA) |
|--------------------|--|---|
| Tx Power | Large | Small |
| Calibration | Difficult | Easy |
| Data processing | <ul style="list-style-type: none">• Raw data• Deconvolution | <ul style="list-style-type: none">• Fourier transform• Superresolution (subspace/ML) |
| Resolution | Fourier | High resolution |



UWB Channel Sounding

Directive antenna vs Array antenna

| |  Directive antenna |  Array antenna |
|-----------------|--|---|
| Tx Power | Small | Large |
| Sync. | Timing | Timing and phase |
| Data processing | <ul style="list-style-type: none">• Raw data• Deconvolution | <ul style="list-style-type: none">• Fourier transform• Superresolution (subspace/ML) |
| Resolution | Fourier | High resolution |

UWB Channel Sounding

Real array vs Synthetic array

| |  Real array |  Synthetic array |
|------------------|---|---|
| Realization | Multiple antennas RF switch | Scanning |
| Measurement time | Short | Long |
| Mutual coupling | To be compensated | None |
| Antenna spacing | Limited by antenna size | No restriction |

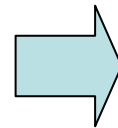
Summary: UWB Sounding Approach

- Double directional model

$$H_{\text{Multipath}}(f, \boldsymbol{\Omega}_{\text{Tx}}, \boldsymbol{\Omega}_{\text{Rx}}) = \sum_{l=1}^L a_l(f) \delta(\boldsymbol{\Omega}_{\text{Tx}} - \boldsymbol{\Omega}_{\text{Tx},l}) \delta(\boldsymbol{\Omega}_{\text{Rx}} - \boldsymbol{\Omega}_{\text{Rx},l}) \exp(-j2\pi f \tau_l)$$

- Architecture

- Frequency domain
- Synthetic array



- VNA
- XY scanner

- Data processing

- ML based super resolution

Summary: UWB Sounding Approach

- Pros and Cons
 - Short range ~ low power handling
 - Output power
 - Cable loss
 - Antenna scanning
 - Static environment
 - No array calibration

SAGE Algorithm for UWB (1)

SAGE Algorithm

- Widely adopted for wideband channel estimation



Novel UWB Signal Model

- Each path has
 - DOA and TOA : independent of the frequency
 - Path gain, phase rotation component : frequency dependent
- UWB signal is expressed as the superposition of conventional wideband signals

SAGE Algorithm for UWB (2)

- SAGE Algorithm

- Search the parameters that maximize log-likelihood
- Reduction of simultaneous search dimension
 - Derivation of complete data from incomplete data (EM)

$$\mathbf{y} \rightarrow \{\mathbf{x}_l\}_{l=1}^L \quad (\text{E-step})$$

$$\arg \max_{\theta} \ln p(\mathbf{x}_l | \theta) \quad \text{for each } \mathbf{x}_l \quad (\text{M-step})$$

- Search in hidden data space = sequential search (SAGE)

SAGE Algorithm for UWB (3)

- Extension of SAGE Algorithm for UWB signal (1)
 - The log-likelihood of UWB signal: **sum of log-likelihood in each subband**

- Log-likelihood function in conventional wideband signal

$$\ln p(\mathbf{x}_l | \theta) = \|\mathbf{x}_l - s \times \mathbf{a}_l(\theta)\|^2$$

s is assumed to be constant !!

- However, in the UWB signal ...

$$\ln p(\mathbf{x}_l | \theta) = \|\mathbf{x}_l - s(f) \times \mathbf{a}_l(\theta)\|^2$$

s is frequency dependent component !!

- s is assumed to be constant within each subband

SAGE Algorithm for UWB (4)

- Extension of SAGE Algorithm for UWB signal (2)

- The log-likelihood of UWB signal:

$$\ln p(\{\mathbf{x}_{l,i}\}_{i=1}^I | \theta) = \sum_{i=1}^I \|\mathbf{x}_{l,i} - s_i \times \mathbf{a}_i(\theta)\|^2$$

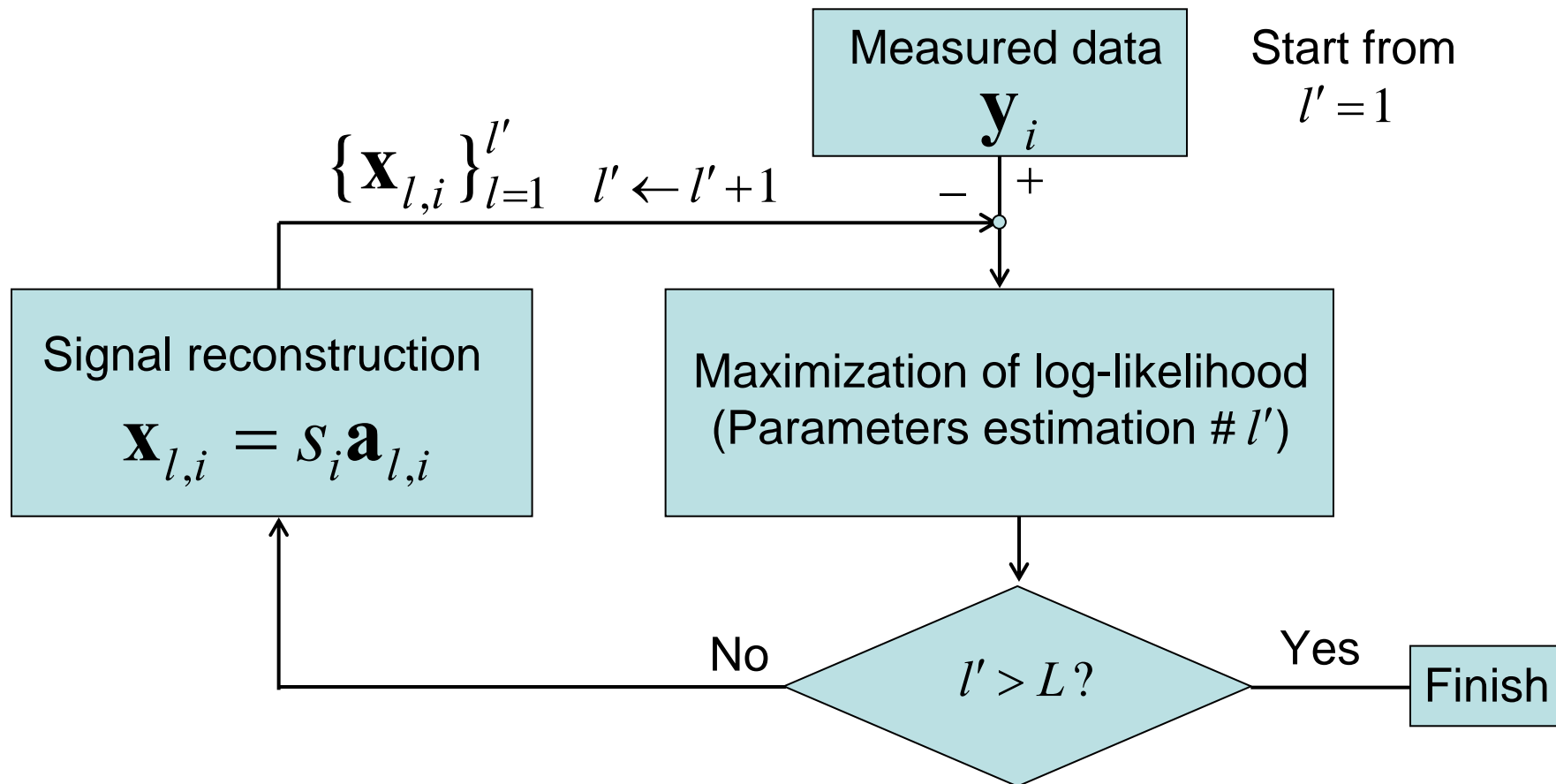
- The frequency dependent spectrum variation can be estimated as well as DoA and DT

- The process of the algorithm can be regarded as the formulation of multi-dimensional matched filter

- There are plenty ways of implementation of search as well as the initialization

SAGE Algorithm for UWB (5)

- One realization of the search (SIC-type)



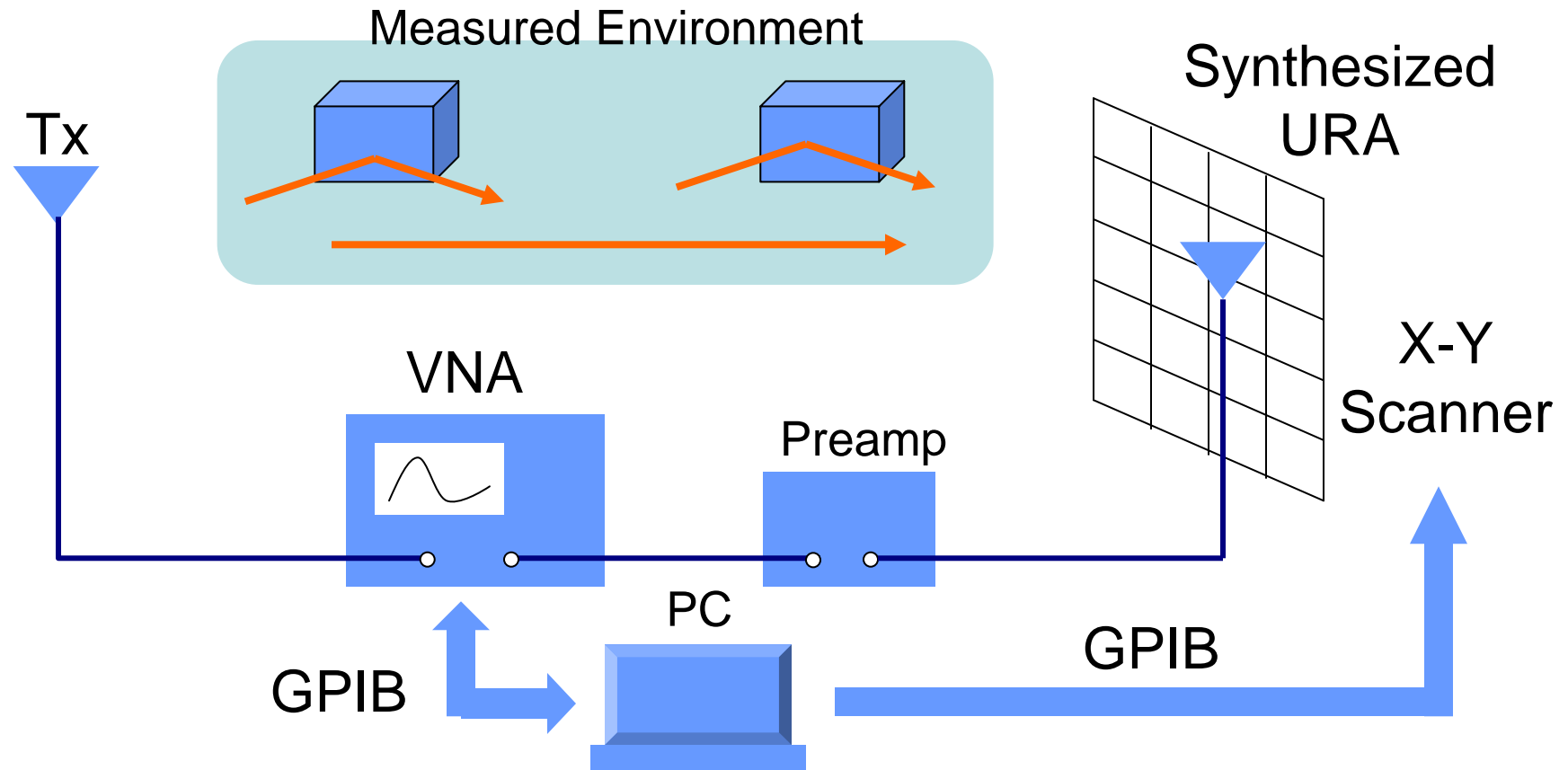
This is equivalent to the EM algorithm of the number of waves = 1.

SAGE Algorithm for UWB (6)

- Sensor-Clean vs. SAGE
 - Sensor-Clean (Cramer et al, 2002)
 - Beamforming + waveform estimation in time domain
 - Applicable even if the transmit waveform is unknown in receiver side
 - Require the time domain data (ex. with Digital Sampling Oscilloscope)
 - SAGE for UWB (Takada)
 - Beamforming + spectrum estimation in frequency domain
 - Applicable only when the transmit waveform is known in receiver side
 - The measurement is possible with Vector Network Analyzer Based system
 - Easy to deconvolute the antenna and propagation phenomena

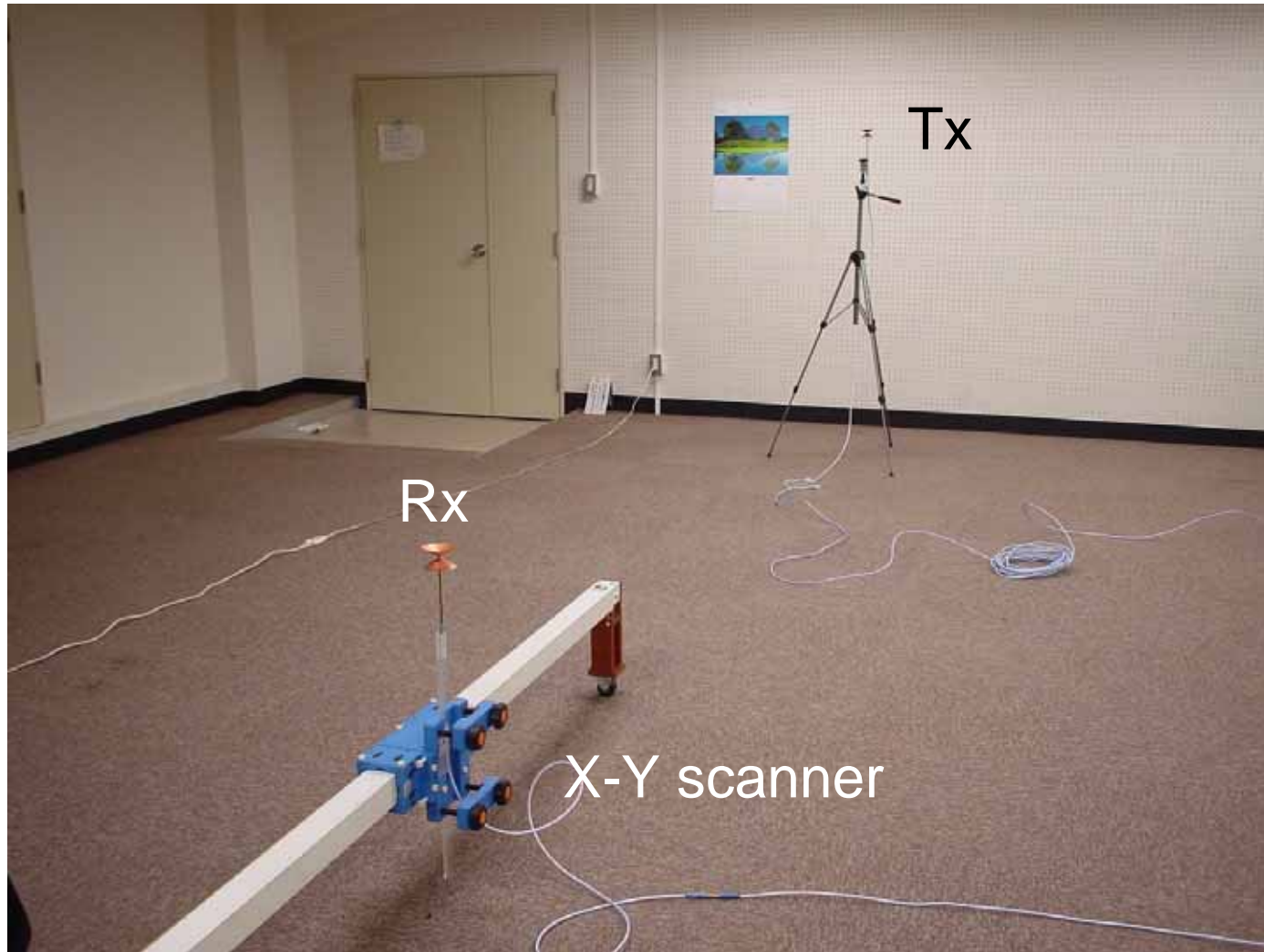
UWB Channel Sounding System

- System configuration: vector network analyzer based
 - Measurement of spatial transfer function automatically



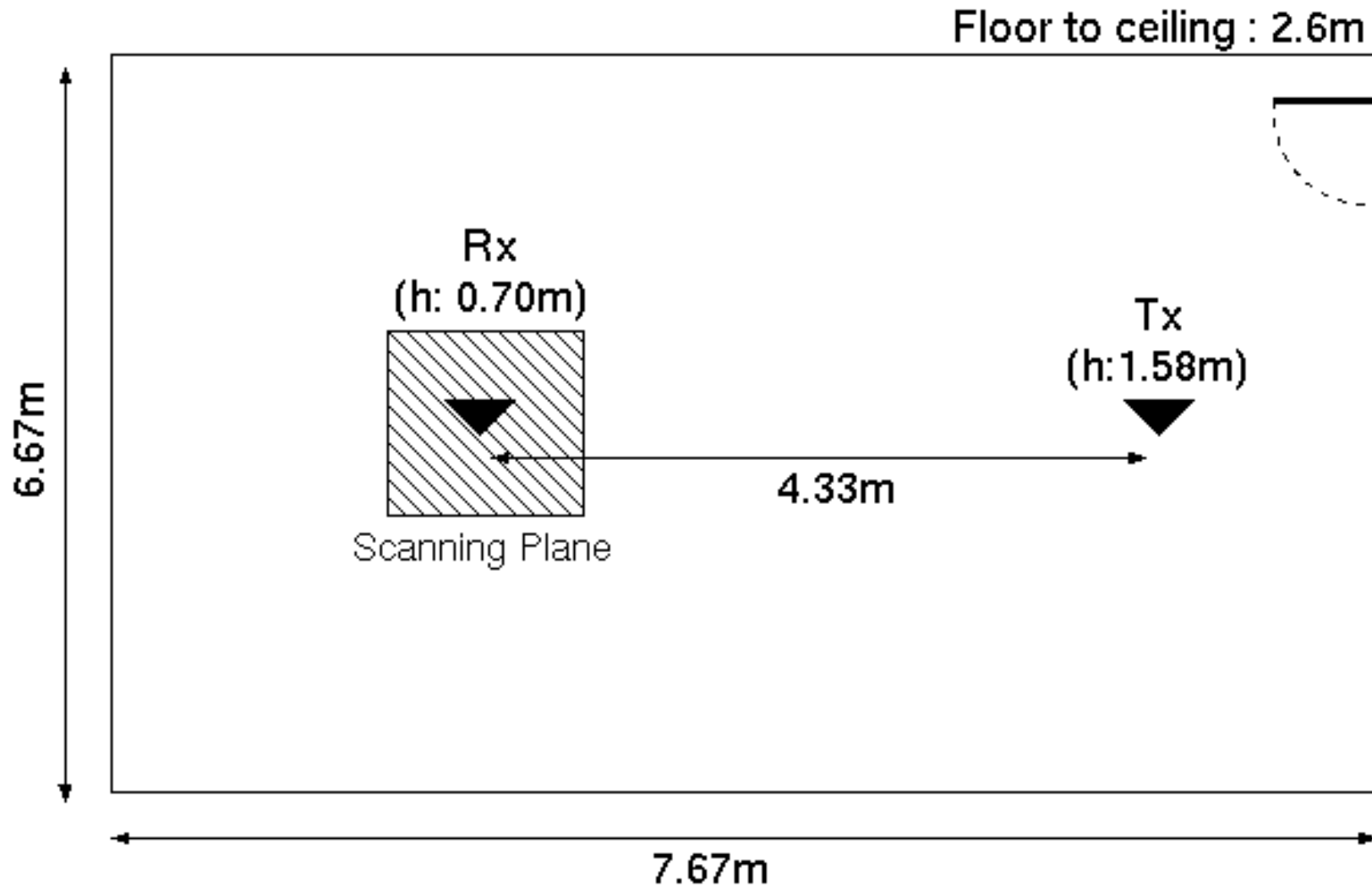
Experiment in an Indoor Environment (1)

- Measurement site: an empty room



Experiment in an Indoor Environment (2)

- Floor plan of the room

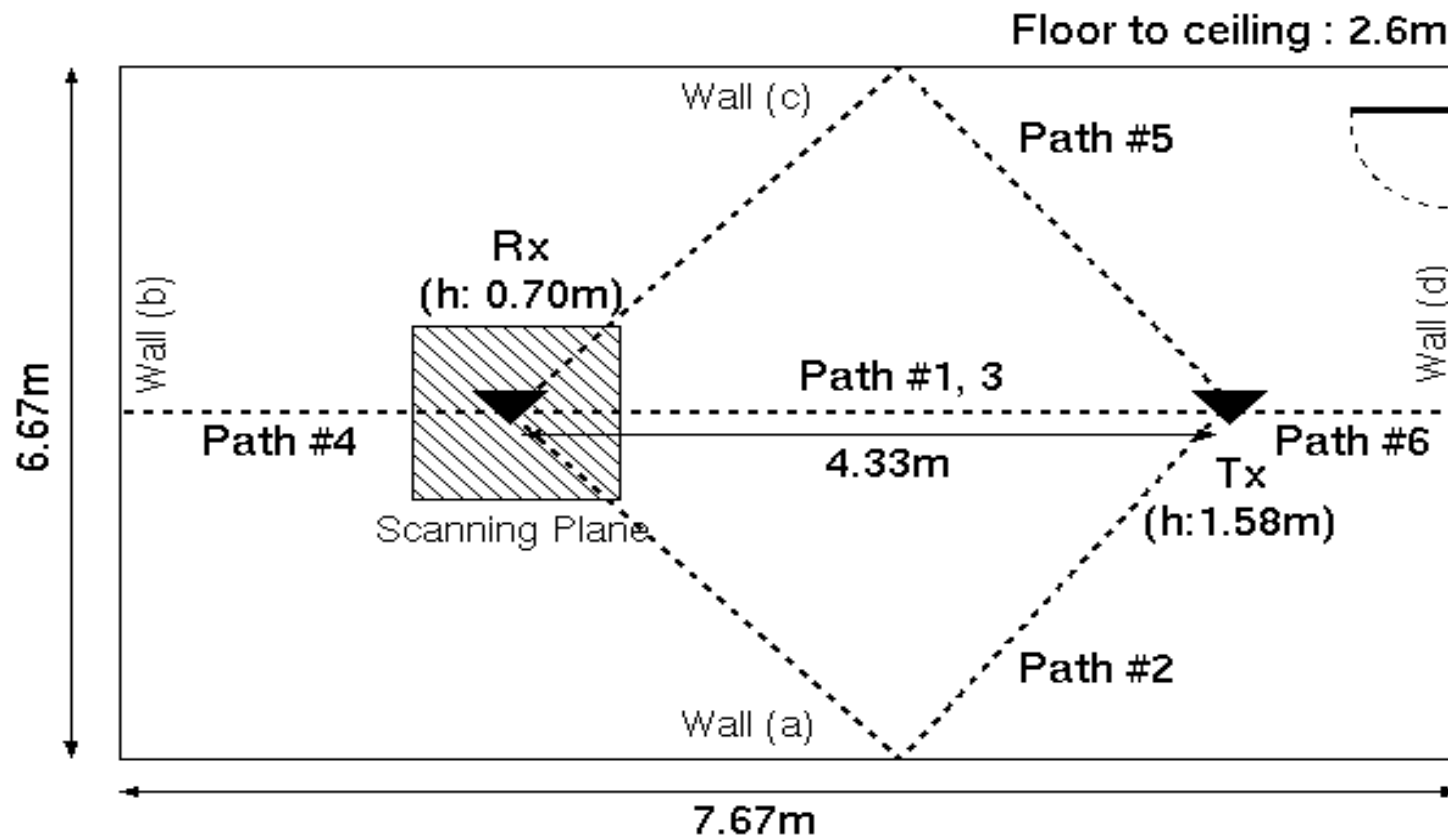


Experiment in an Indoor Environment (3)

- Estimated parameters : DoA (Az, EI), DT
- Measured data :
 - Spatially 10 by 10 points at Rx
 - 801 points frequency sweeping from 3.1 to 10.6 [GHz] (sweeping interval: 10 [MHz])
- Antennas : Biconical antennas for Tx and Rx
- Calibration : Function of VNA, back-to-back
- IF Bandwidth of VNA : 100 [Hz]
- Wave polarization : Vertical - Vertical
- Bandwidth of each subband : 800 [MHz]

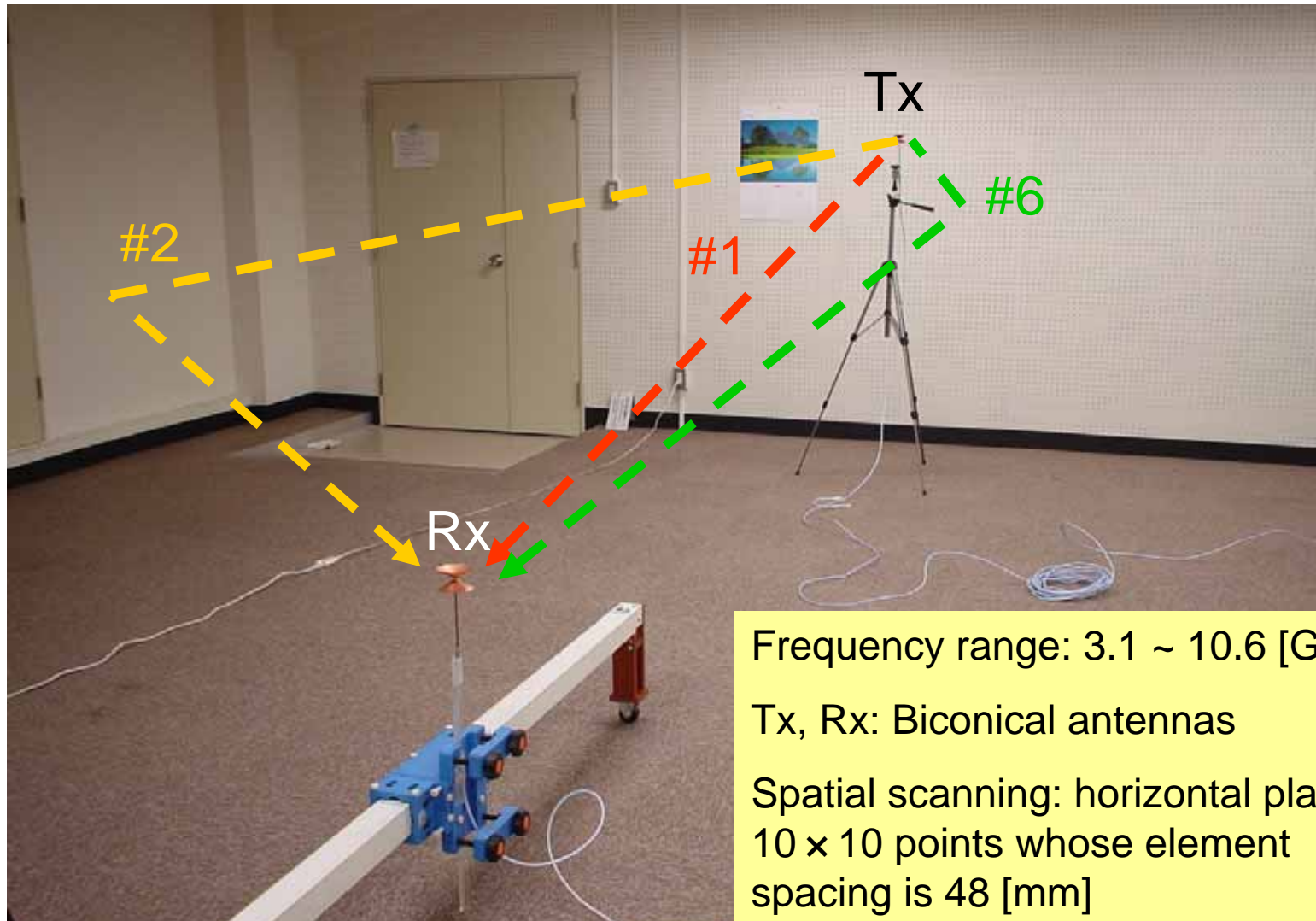
Measurement Result (1)

- The result of ray path identification



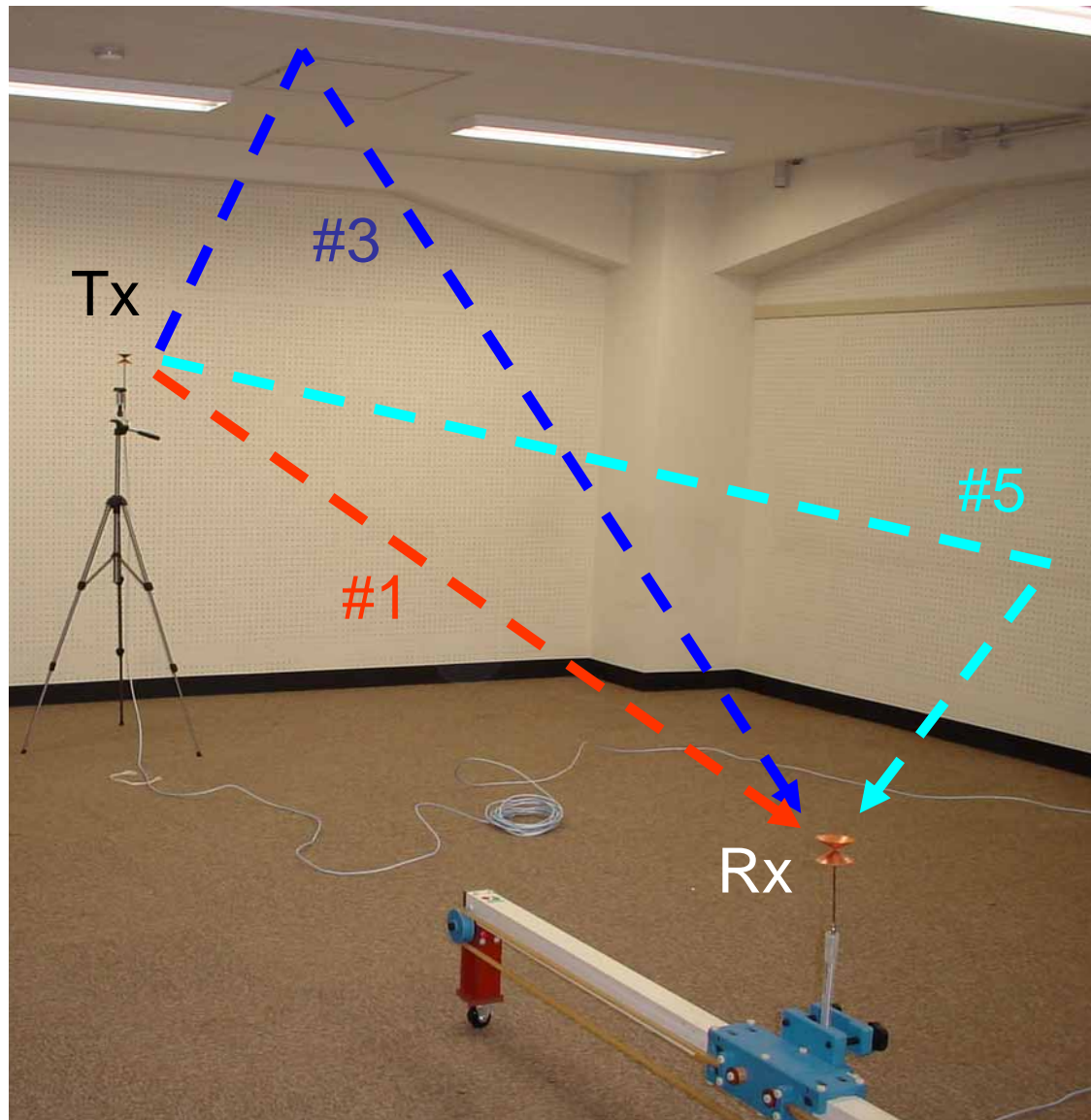
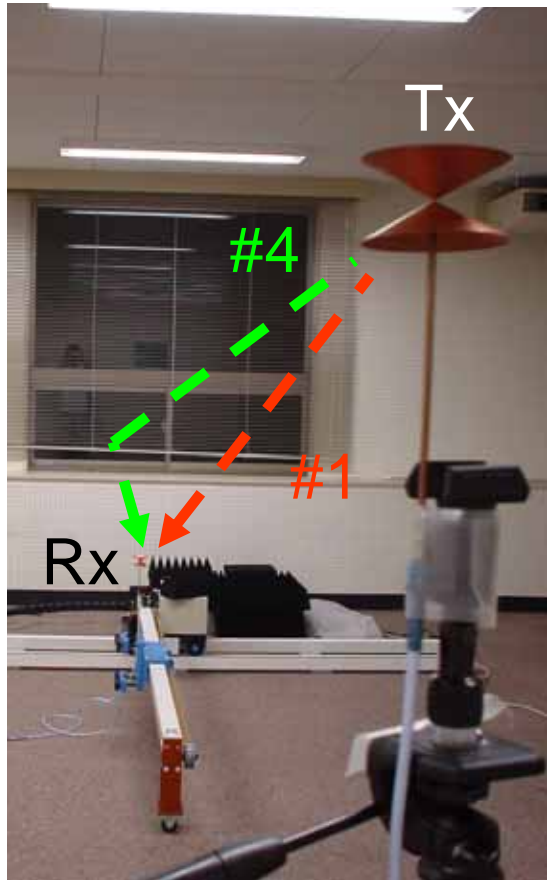
There 6 waves detected and are almost specular waves.

Measurement Result (2)



6 specular waves were observed.

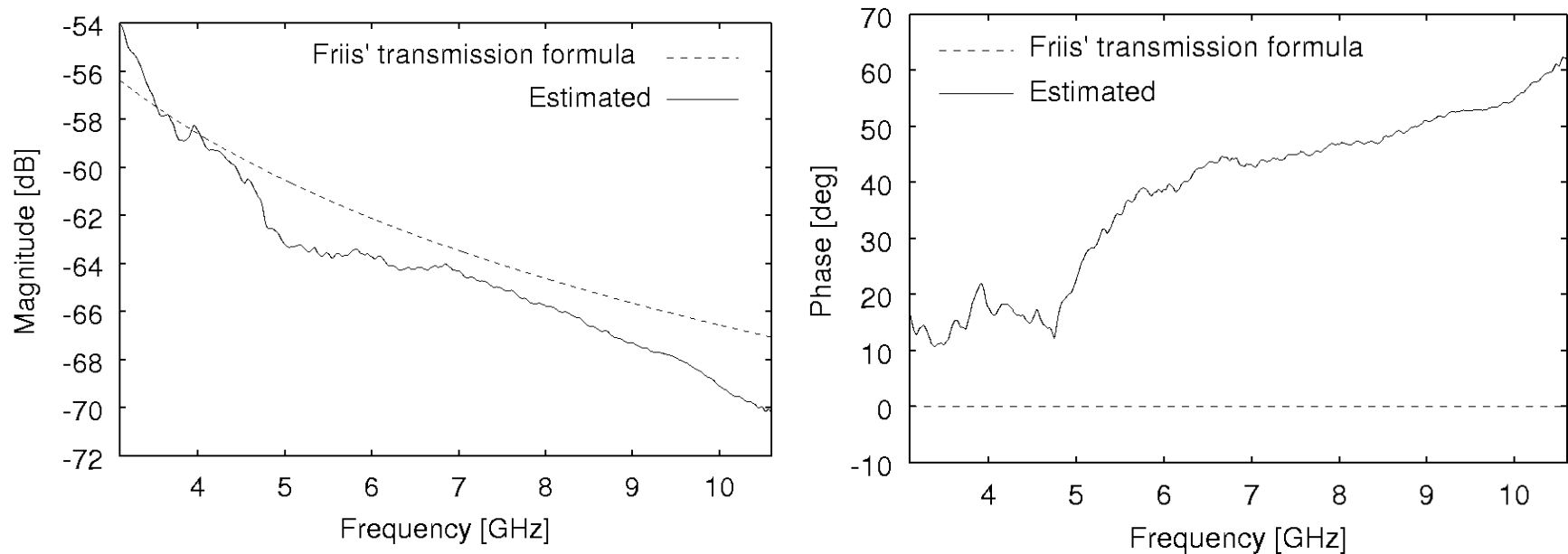
Measurement Result (3)



#4 is a reflection from the back of Rx

Measurement Result (4)

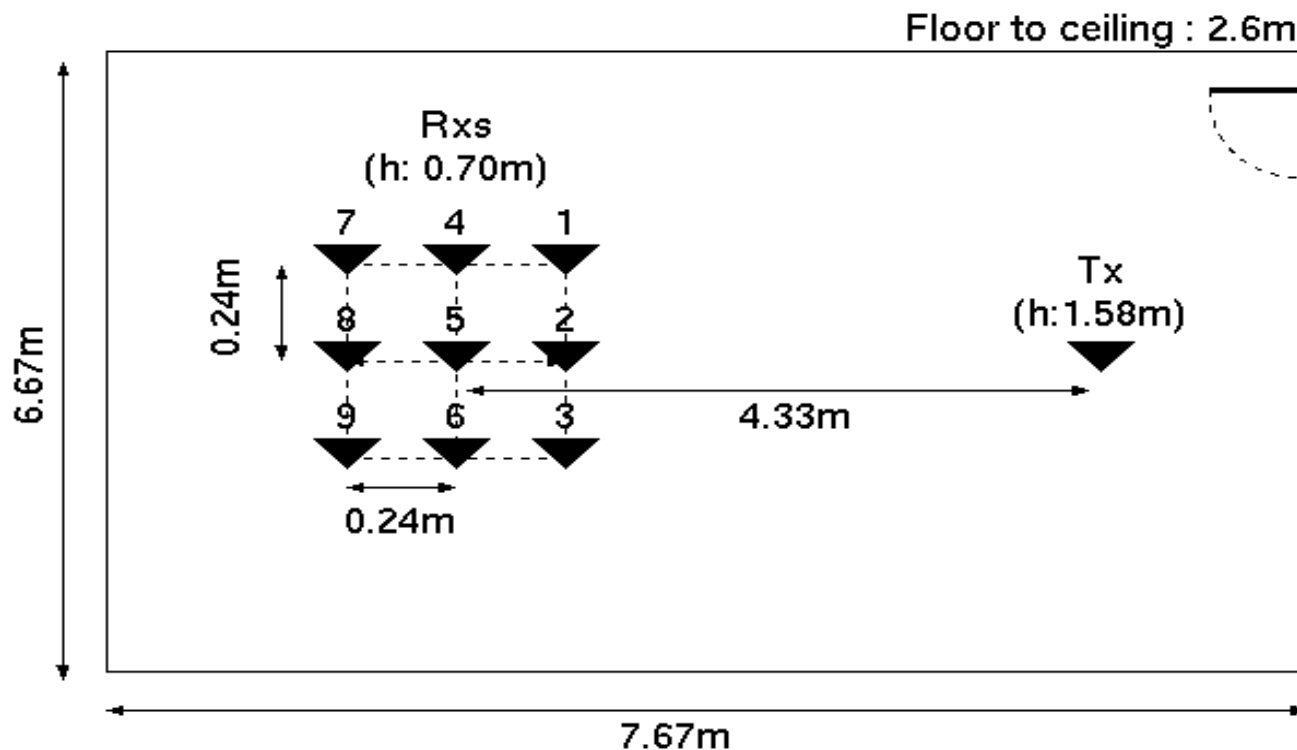
- Extracted spectrum of direct wave



- Transfer functions of antennas are already deconvolved.
- The phase component is the deviation from free space phase rotation (ideally flat).

Experiment in an Indoor Environment (4)

- Comparison of the measurement result in 9 different Rx position



The path type detected in each measurement was almost same.

Measurement Result (5)

- Estimated source position for direct wave

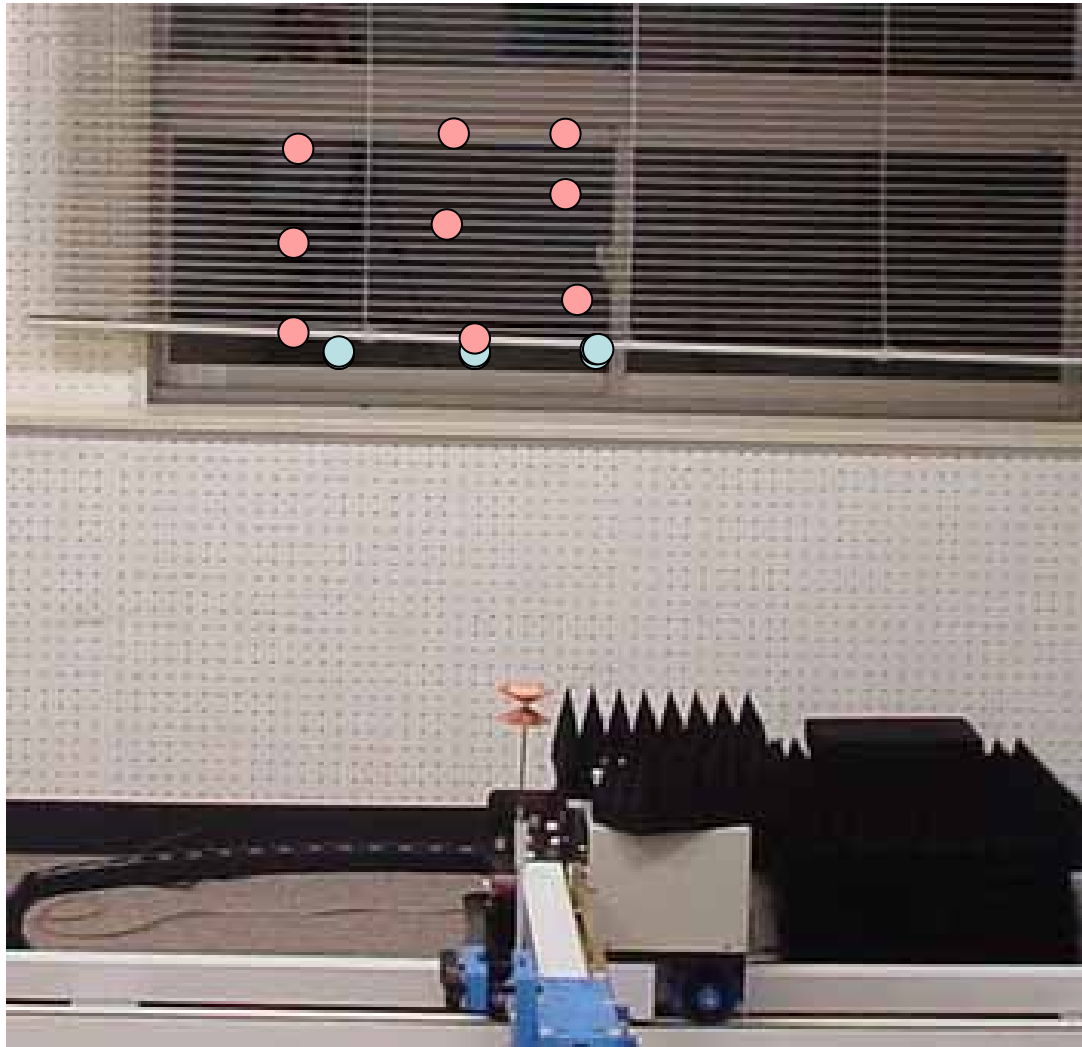


Maximum deviation is 17cm from source point.

● Estimated by measurement

Measurement Result (6)

- Estimated reflection points in back wall reflection



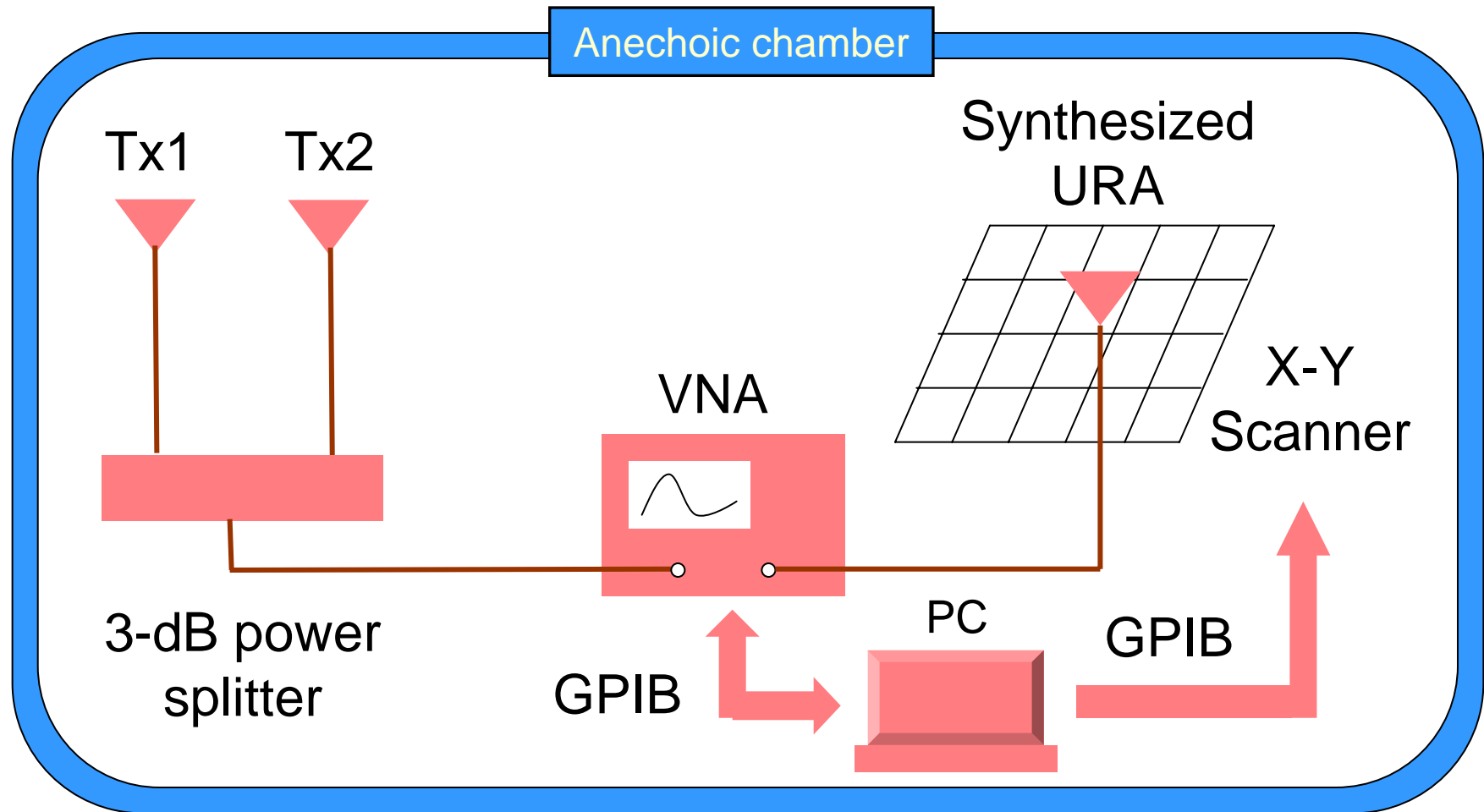
All the reflection points are above those predicted by GO.

- Predicted by GO
- Estimated by measurement

Discussion

- Some problems have been appeared.
 - 2 ~ 4 spurious waves detected during the estimation of 6 waves
 - Residual components after removing dominant paths
 - Signal model error (plane or spherical)
 - Estimation error based on inherent resolution of the algorithm implementation
 - Many distributed source points (diffuse scattering)
- ➔ Further investigation in simple environment

Performance Evaluation in Anechoic Chamber



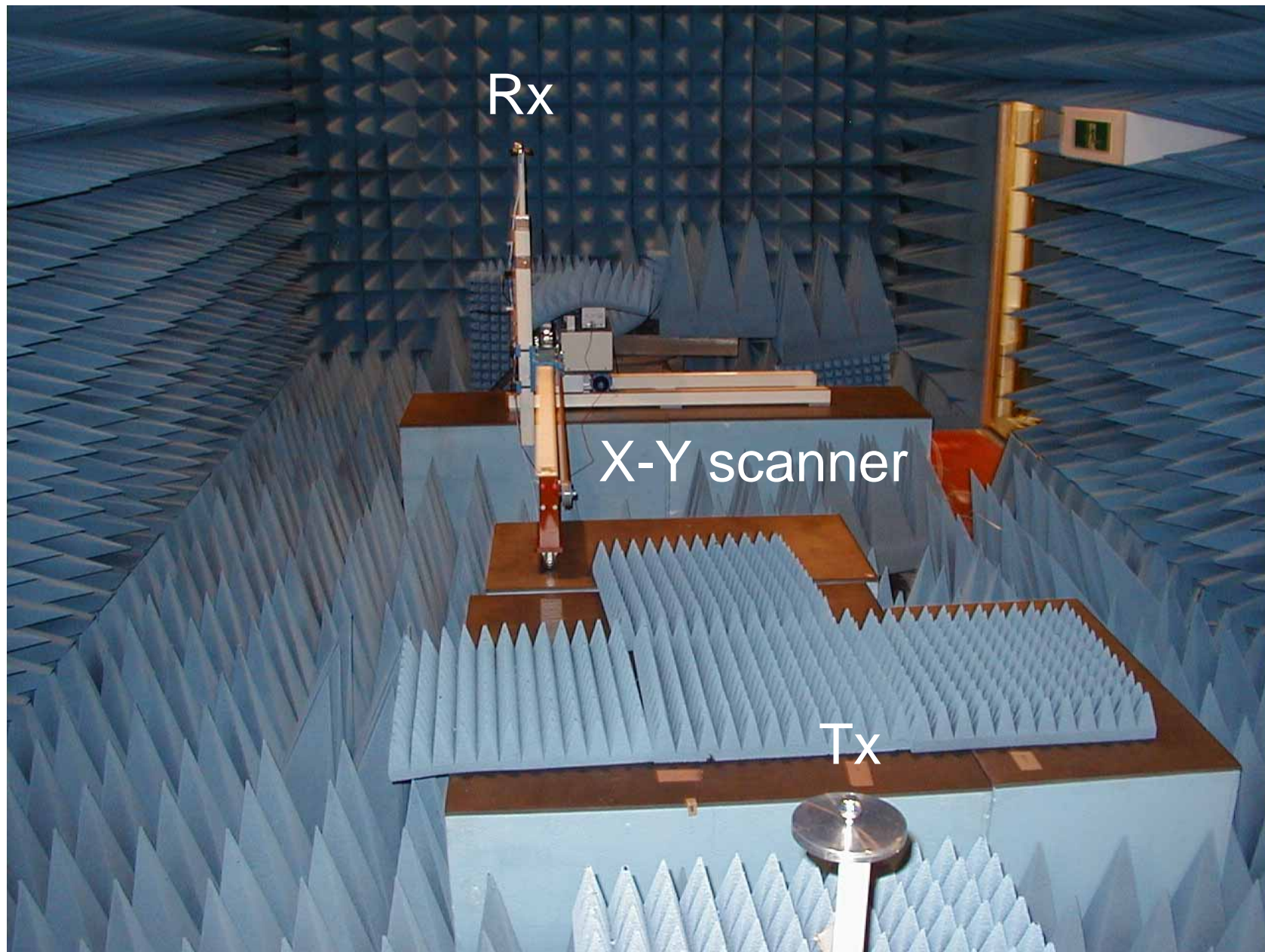
Specifications of Experiment

- Frequency : 3.1 ~ 10.6 GHz
 - 0.13 ns Fourier resolution
- Antenna scanning plane : 432 mm square in horizontal plane
 - 10 deg Fourier resolution
 - 48 mm element spacing
(less than half wavelength @ 3.1 GHz)
- Wideband monopole antennas were used
 - Variation of group delay < 0.1 ns within the considered bandwidth
- SNR at receiver : About 25 dB

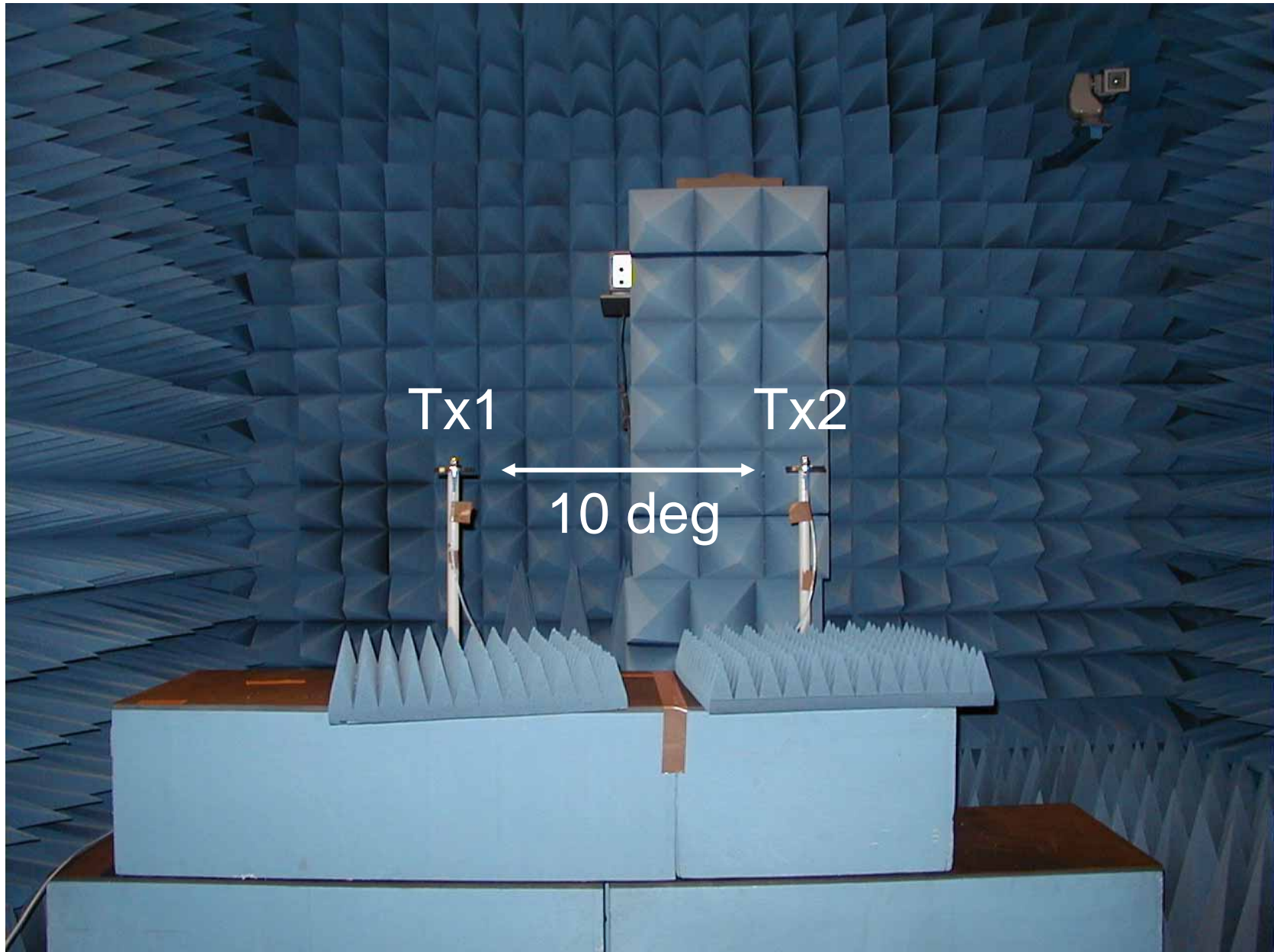
Aim of Anechoic Chamber Test

- Evaluation of spatio-temporal resolution
 - Separation and detection of two waves that
 - Spatially 10 deg different and same DT
 - Temporally 0.67 ns (= 20 cm) different and same DoA

Setup of Experiment

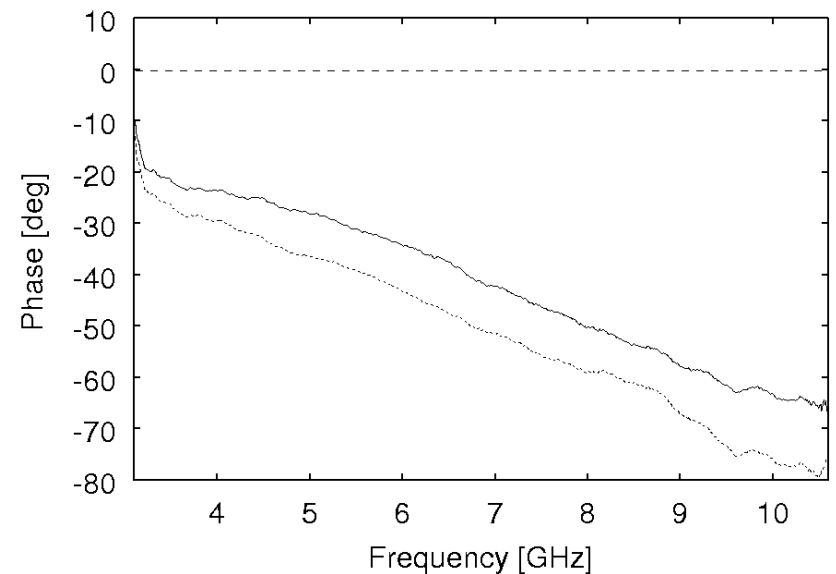
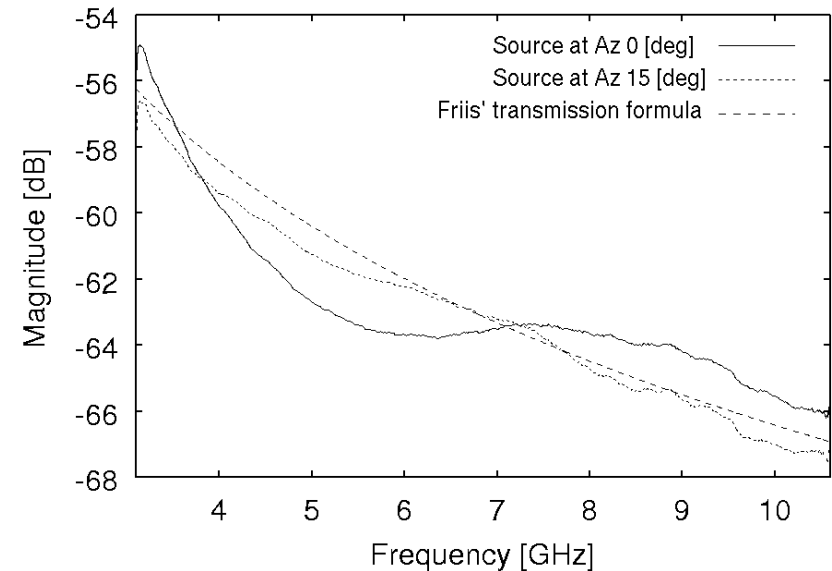


Spatial Resolution Test (1)

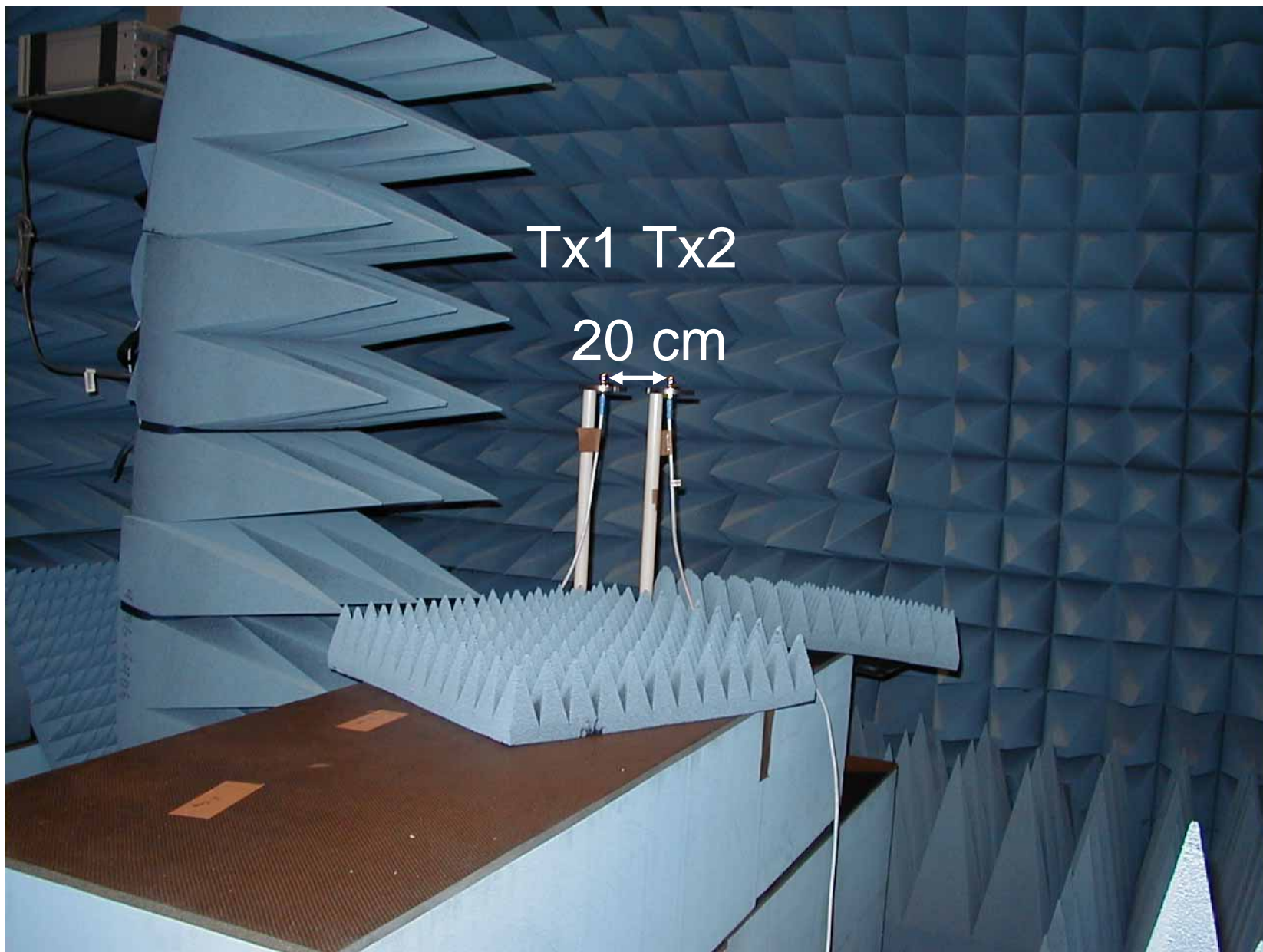


Spatial Resolution Test (2)

- 10 deg separated waves are accurately separated.
 - Parameters and spectra are accurately estimated.
 - The estimated phase denotes a deviation from free space phase rotation (~ 3 mm).
 - Antenna characteristics are already deconvolved.



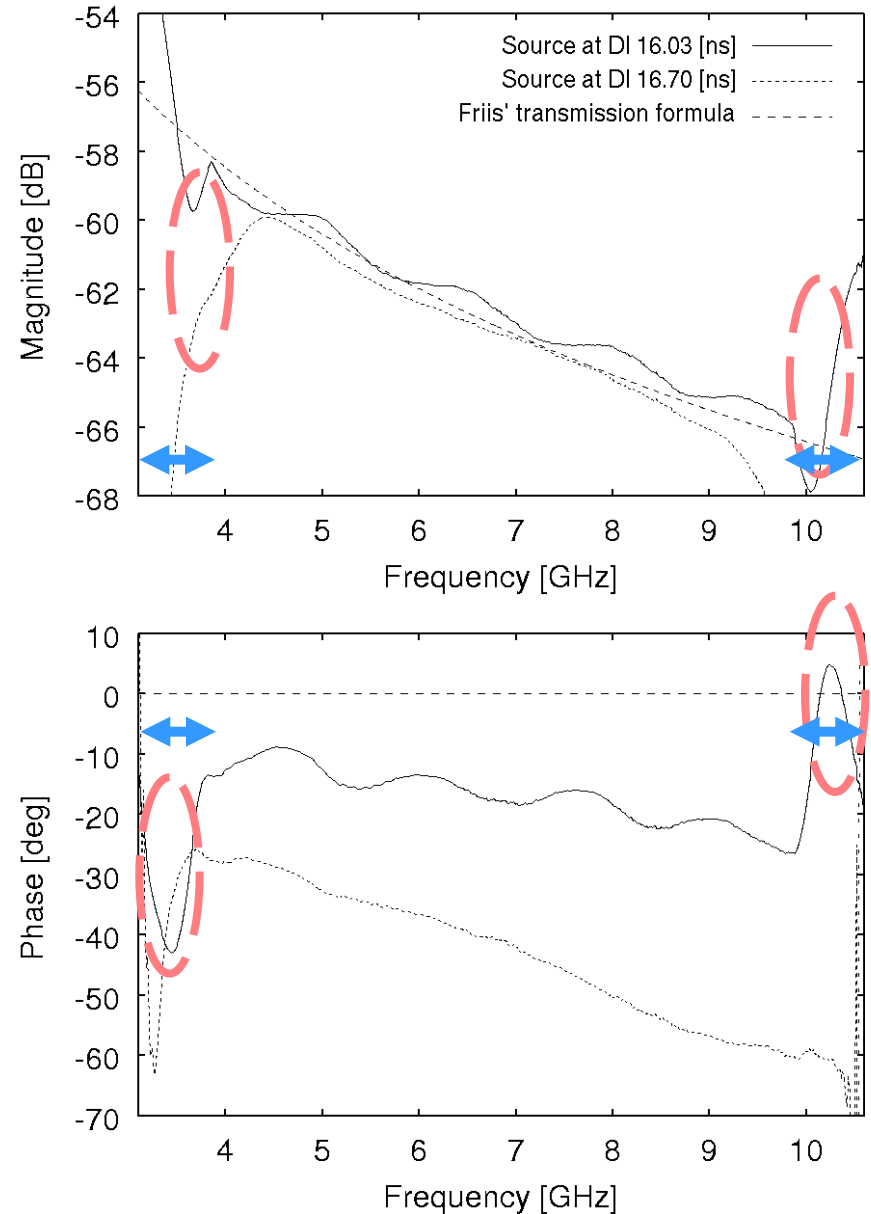
Temporal Resolution Test (1)



Temporal Resolution Test (2)

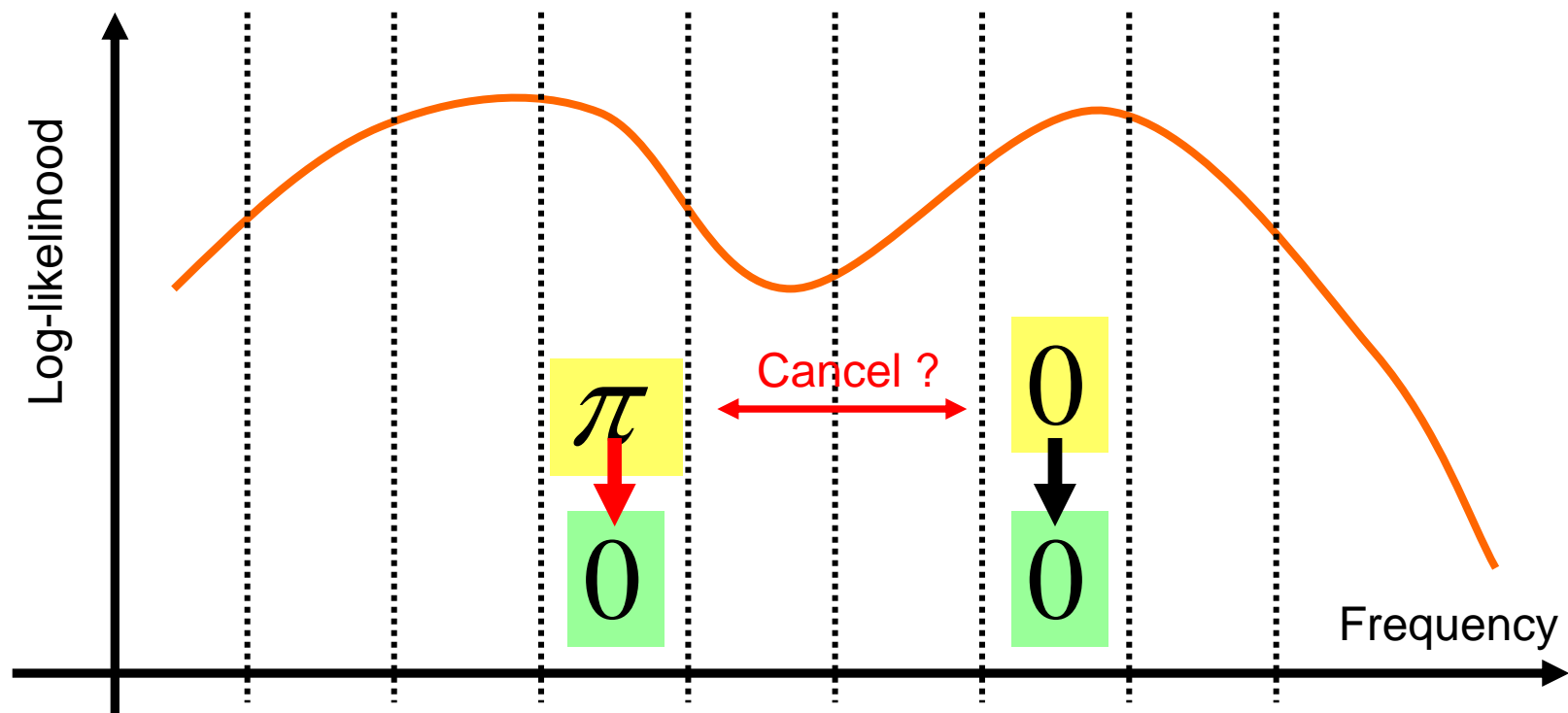
- 0.67 ns separated waves are accurately resolved.
 - Subband width : 1.5 GHz
 - Spectrum estimation is impossible in the higher and lower frequency region of

$$\left(\frac{1}{\Delta\tau = 0.67 [\text{ns}]} \right) / 2 = 0.75 [\text{GHz}]$$



Subband Processing (1)

- ... relieves a bias of parameter estimation due to amplitude and phase fluctuation within the band
- Tradeoff between the resolution and accuracy of parameter estimation: **some optimization is needed !!**



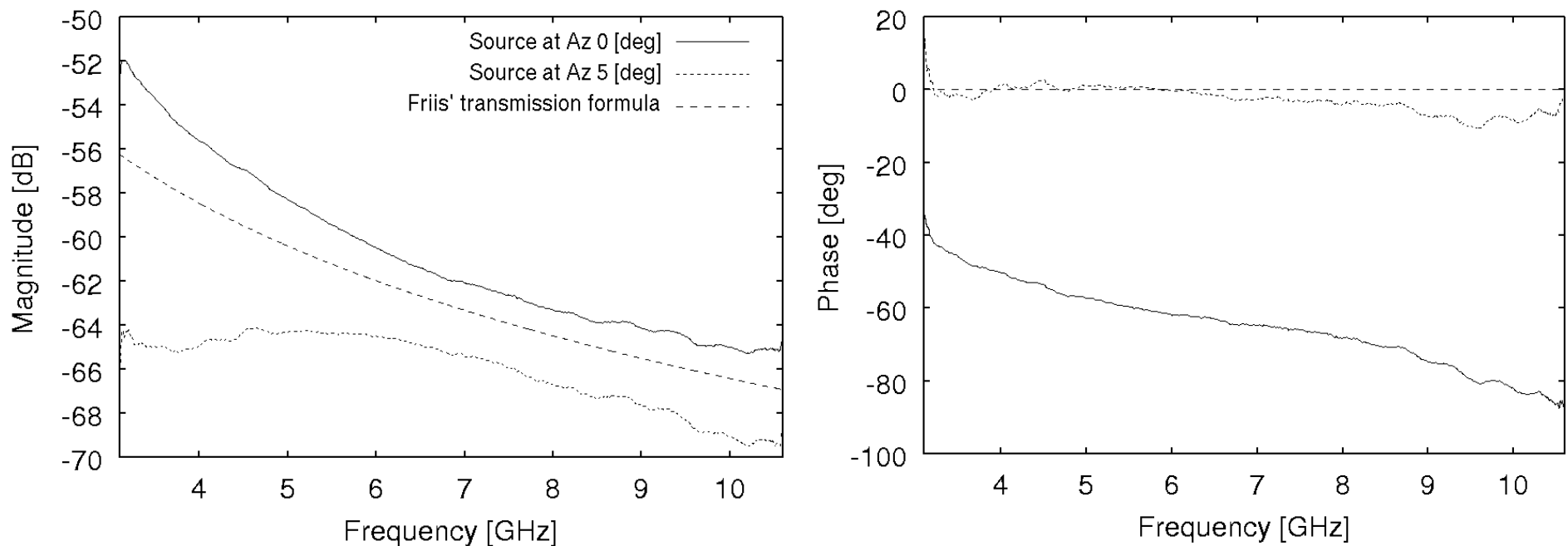
Subband Processing (2)

- How to choose the optimum bandwidth of subband?
 - Suppose two waves are $\Delta\theta$ and $\Delta\tau$ separated

| | | Angle resolution : θ_{res} | |
|---|----------------------------------|--|--------------------------------------|
| | | $\theta_{\text{res}} < \Delta\theta$ | $\theta_{\text{res}} > \Delta\theta$ |
| Delay resolution τ_{res} | $\tau_{\text{res}} < \Delta\tau$ | Bandwidth within which deviation of antennas and propagation characteristics is sufficiently small | $\approx \frac{1}{\Delta\tau}$ |
| | $\tau_{\text{res}} > \Delta\tau$ | | Impossible to resolve |

Subband Processing (3)

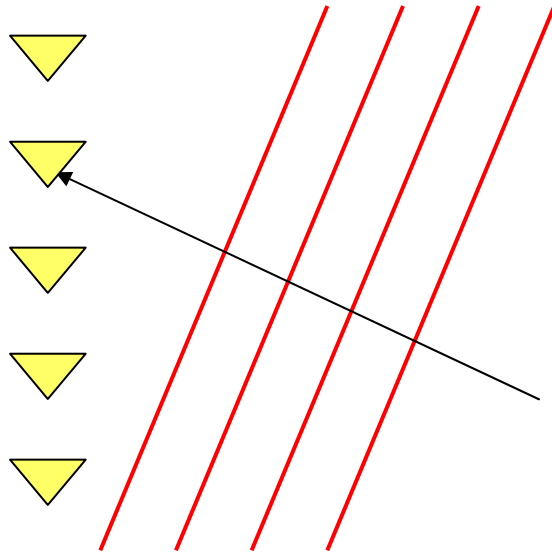
- Behavior for the detection of two waves closer than the inherent resolution of the algorithm
 - Regard two waves as one wave (ex. same incident angle)
 - Two separated waves, but biased estimation of power (ex. 5 deg different incident angles)



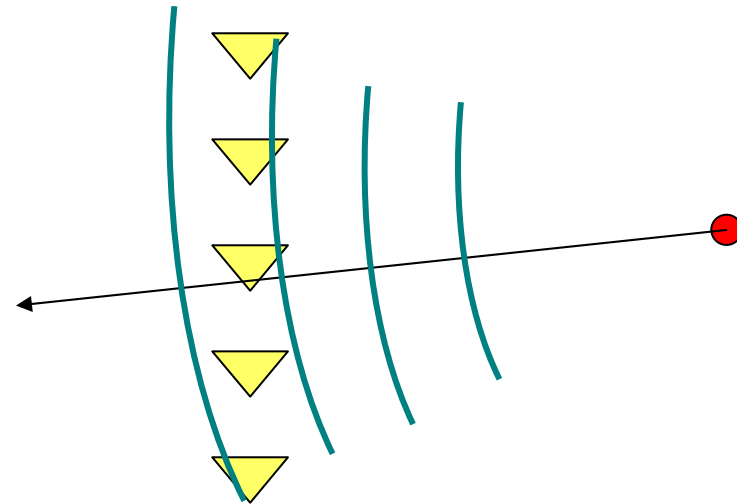
Deconvolution of Antenna Patterns

- Deconvolution of antennas
 - Construction of channel models independent of antenna type and antenna configuration
 - Deconvolution is post-processing (from the estimated spectrum by SAGE)
 - Simple implementation rather than the deconvolution during the search

Spherical vs Plane Wave Models (1)



Plane wave incidence
(far field incidence)

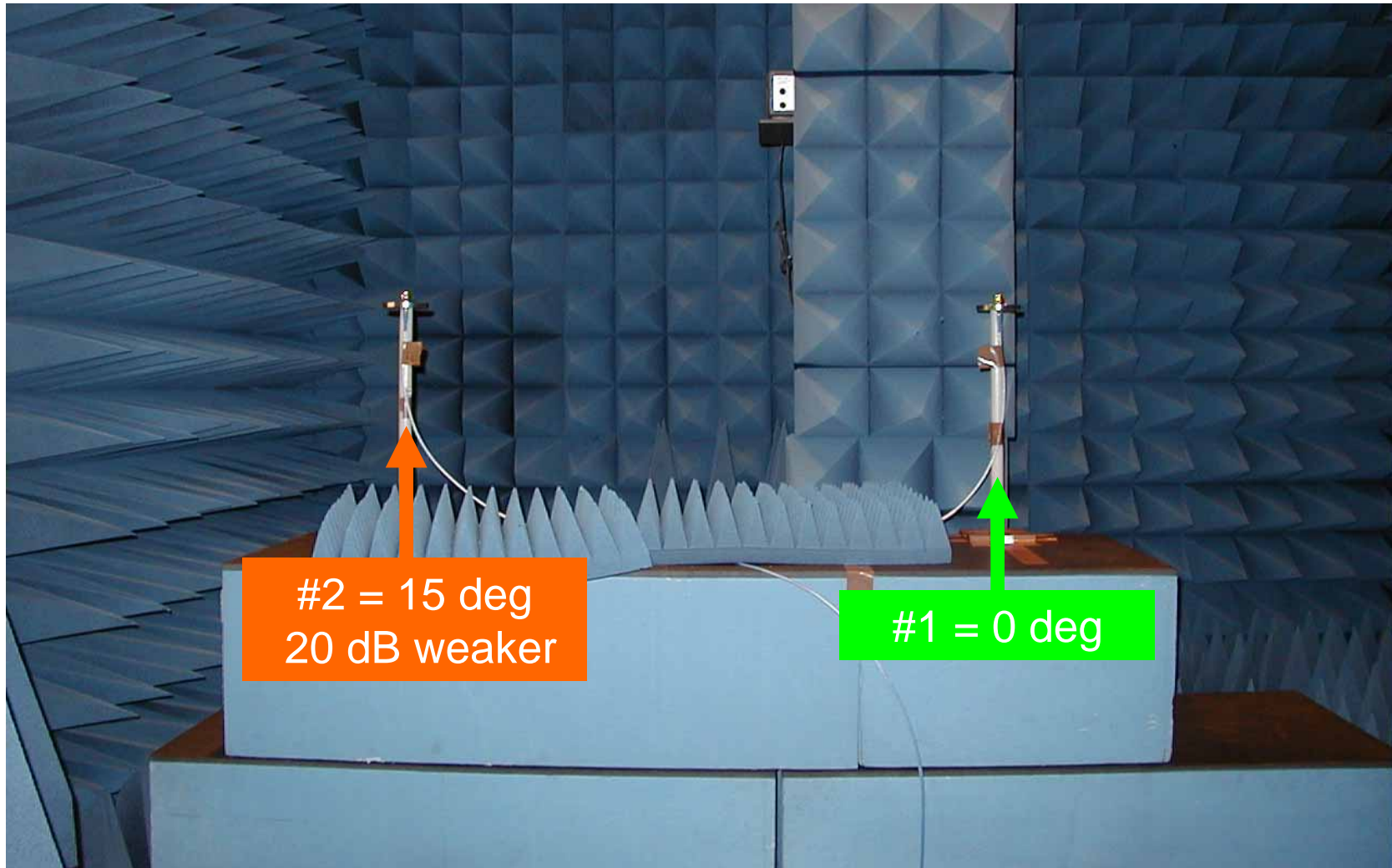


Spherical wave incidence
(radiation from point source)

- How these models affect for the accurate estimation?
 - Spurious (ghost path) and detection of weak paths
 - Empirical evaluation of model accuracy

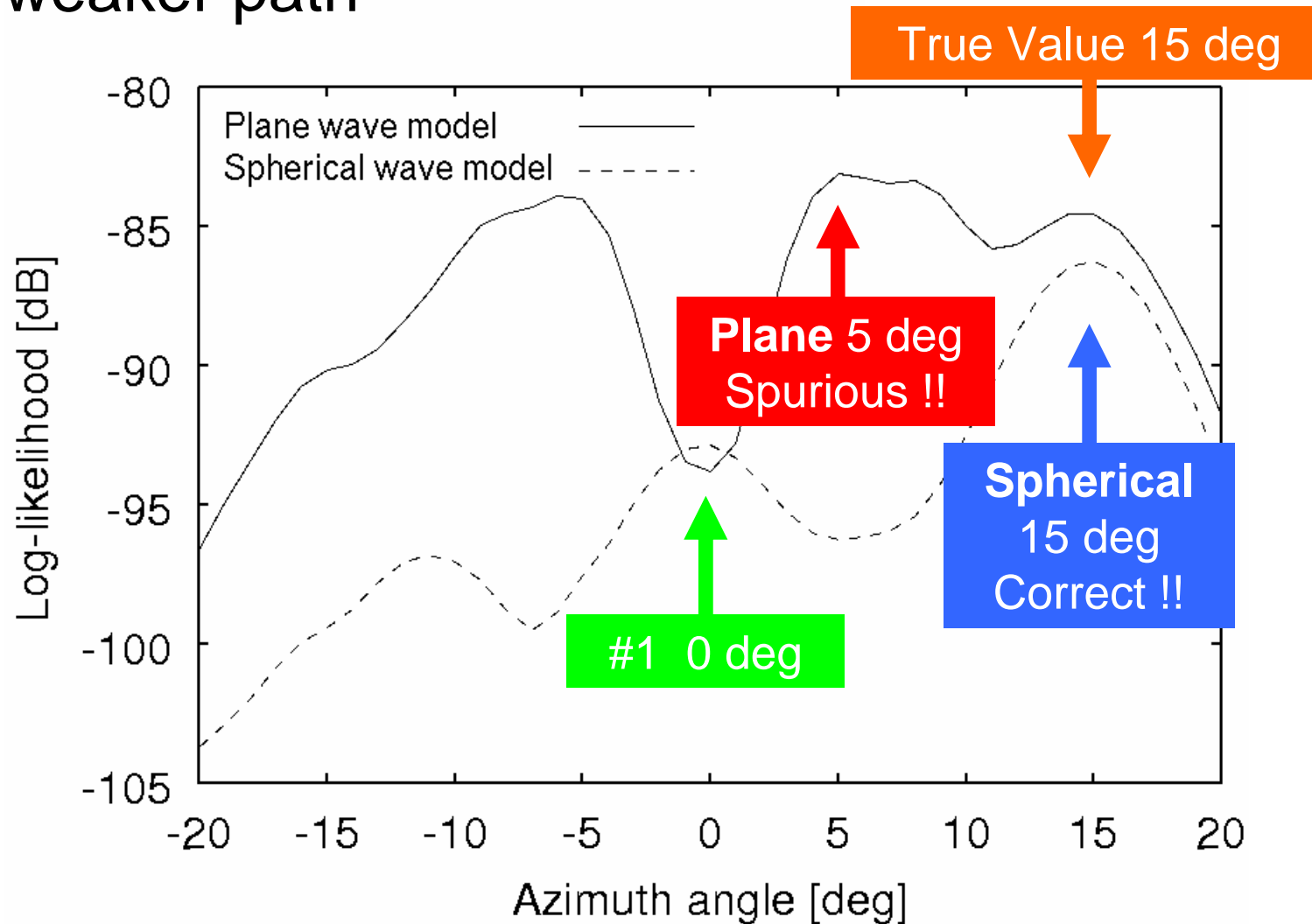
Spherical vs Plane Wave Models (2)

- Detection of 20 dB different two waves
 - Is a weaker source correctly detected?



Spherical vs Plane Wave Models (3)

- Log-likelihood spectrum in the detection of weaker path



Summary of Evaluation Works (1)

- Evaluation of the proposed UWB channel sounding system in an anechoic chamber
 - Resolved spatially 10 deg, temporally 0.67 ns separated waves
 - Spectrum estimation is partly impossible in the highest and lowest frequency regions of $\frac{1}{2\Delta\tau}$.
 - The algorithm treats two waves closer than inherent resolution as one wave, or results in biased power estimation even if they are separated.

Summary of Evaluation Works (2)

- For reliable UWB channel estimation with SAGE algorithm
 - An optimum way to choose the bandwidth of subband
 - The number of waves estimation is done by SIC- type procedure
- Deconvolution of antennas effects from the results of SAGE
 - For channel models independent of antennas

Summary of Evaluation Works (3)

- Spherical incident wave model is more robust than plane wave incident model
 - Spurious reduction is expected
 - Effective in the detection of weaker path

Summary of This Talk

- Antennas and propagation of UWB
 - Necessity of double directional propagation model
- UWB double directional sounder
 - VNA
 - XY scanner
 - ISI-SAGE (ML based)
- Initial indoor experiment
- Performance evaluation

Future Tasks

- Double directional and polarimetric extension
 - Double directional measurement has started.
 - Extension of estimation program to SIMO to MIMO.
- More field measurements
 - Office
 - Home

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Notice

- The slides include some recent unpublished results, and re-distribution of the slides is not permitted.